

MCT344/MCT342/CSE373/CSE471

# Industrial Robotics

## *Lecture 3: Forward Kinematics for Robotics*

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# Introduction

- The problem of manipulator kinematics is to describe the motion of a manipulator without consideration of the forces and torques causing the motion.
- The forward kinematics problem for serial link manipulators is to determine the position and orientation of the end effector given the values for the joint variables of the robot.
- This problem is easily solved by attaching coordinate frames to each link of the robot and expressing the relationships among these frames as homogeneous transformations.
- We use a systematic procedure, known as the **Denavit-Hartenberg** convention, to attach these coordinate frames to the robot.
- The position and orientation of the robot end effector is then reduced to a matrix multiplication of homogeneous transformations.

# Kinematic Chains

- A robot manipulator is composed of a set of links connected together by joints.
- The joints can either be very simple, such as a revolute joint or a prismatic joint, or they can be more complex, such as a ball and socket joint.
- The difference between the two situations is that in the first instance the joint has only a single degree-of-freedom of motion.
- In contrast, a ball and socket joint has two degrees of freedom.
- It is assumed throughout that **all joints have only a single degree of freedom.**
- Since joints such as a ball and socket joint (two degrees of freedom) or a spherical wrist (three degrees of freedom) can always be thought of as a **succession of single degree-of-freedom joints with links of length zero in between.**

# Kinematic Chains

- A robot manipulator with  $n$  joints will have  $n+1$  links, since each joint connects two links.
- We number the joints from  $1$  to  $n$ , and we number the links from  $0$  to  $n$ , starting from the base.
- By this convention, joint  $i$  connects link  $i-1$  to link  $i$ .
- We will consider the location of joint  $i$  to be fixed with respect to link  $i-1$ .
- When joint  $i$  is actuated, link  $i$  moves.
- Link  $0$  (the first link or base) is fixed, and does not move when the joints are actuated.
- We attach a coordinate frame rigidly to each link. In particular, we attach  $o_i x_i y_i z_i$  to link  $i$ .
- When joint  $i$  is actuated, link  $i$  and its attached frame,  $o_i x_i y_i z_i$ , experience a resulting motion.
- The frame  $o_0 x_0 y_0 z_0$ , which is attached to the robot base, is referred to as the base frame, inertial frame or world frame.

# Kinematic Chains

- $A_i$  is the homogeneous transformation matrix that gives the position and orientation of  $o_i x_i y_i z_i$  with respect to  $o_{i-1} x_{i-1} y_{i-1} z_{i-1}$ .
- $A_i$  is a function of only a single joint variable, namely  $q_i$ .

*Homogeneous Transformation Matrix:*

$$A_i = A_i(q_i)$$

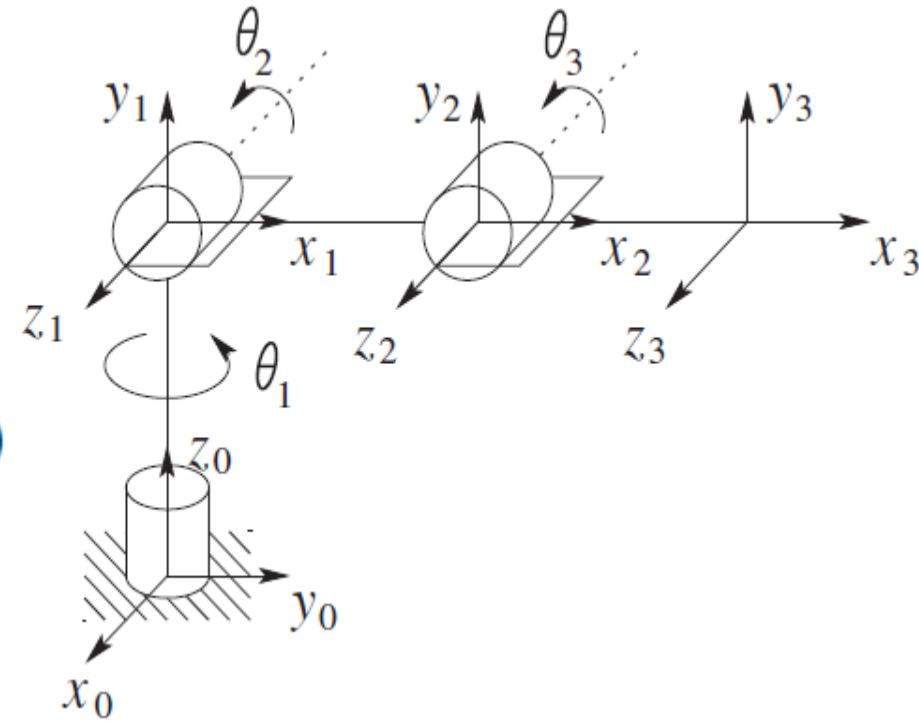
$$H = \begin{bmatrix} R_n^0 & o_n^0 \\ 0 & 1 \end{bmatrix}$$

*The position and orientation of the end effector in the inertial frame are given by the product:*

$$H = T_n^0 = A_1(q_1) \cdots A_n(q_n)$$

*Each homogeneous transformation  $A_i$  is of the form:*

$$A_i = \begin{bmatrix} R_i^{i-1} & o_i^{i-1} \\ 0 & 1 \end{bmatrix}$$



# The Denavit-Hartenberg Convention

$$q_i = \begin{cases} \theta_i & \text{if joint } i \text{ is revolute} \\ d_i & \text{if joint } i \text{ is prismatic} \end{cases}$$

$$A_i = \text{Rot}_{z,\theta_i} \text{Trans}_{z,d_i} \text{Trans}_{x,a_i} \text{Rot}_{x,\alpha_i}$$

$$= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i} & 0 & 0 \\ s_{\theta_i} & c_{\theta_i} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\times \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & c_{\alpha_i} & -s_{\alpha_i} & 0 \\ 0 & s_{\alpha_i} & c_{\alpha_i} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i}c_{\alpha_i} & s_{\theta_i}s_{\alpha_i} & a_i c_{\theta_i} \\ s_{\theta_i} & c_{\theta_i}c_{\alpha_i} & -c_{\theta_i}s_{\alpha_i} & a_i s_{\theta_i} \\ 0 & s_{\alpha_i} & c_{\alpha_i} & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

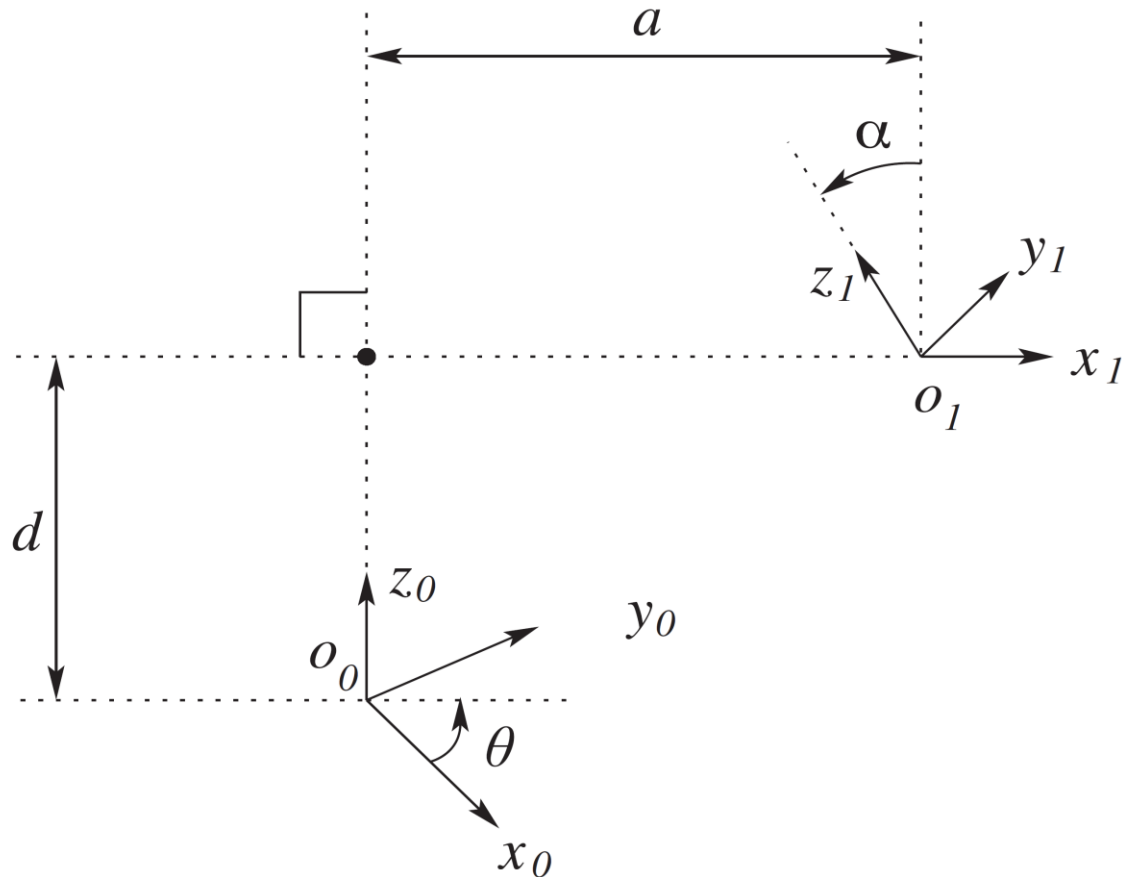
$a_i$	Link Length
$\alpha_i$	Link Twist
$d_i$	Link Offset
$\theta_i$	Joint Angle

Since the matrix  $A_i$  is a function of a single variable, three of the above four quantities are constant for a given link, while the fourth parameter,  $\theta_i$  for a revolute joint and  $d_i$  for a prismatic joint, is the joint variable.

# The Denavit-Hartenberg Convention

## *Existence and Uniqueness*

There exists a unique homogeneous transformation matrix  $A$  that takes the coordinates from frame  $1$  into those of frame  $0$ .



$a_i$	Link Length
$\alpha_i$	Link Twist
$d_i$	Link Offset
$\theta_i$	Joint Angle

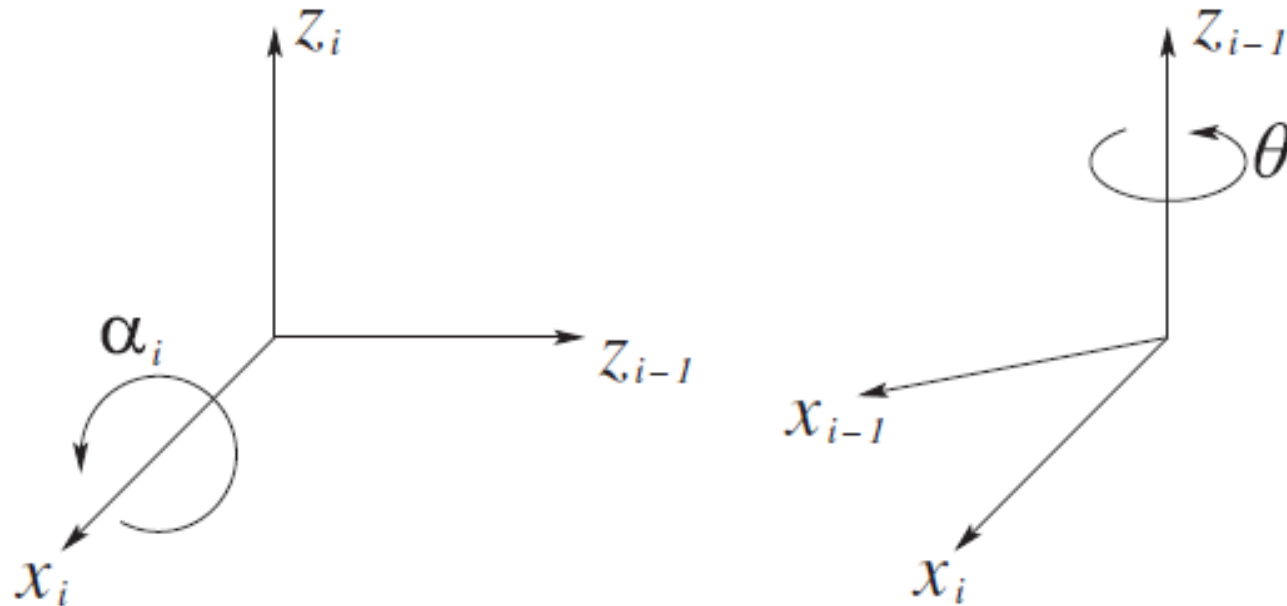
(DH1) The axis  $x_1$  is perpendicular to the axis  $z_0$ .

(DH2) The axis  $x_1$  intersects the axis  $z_0$ .

# The Denavit-Hartenberg Convention

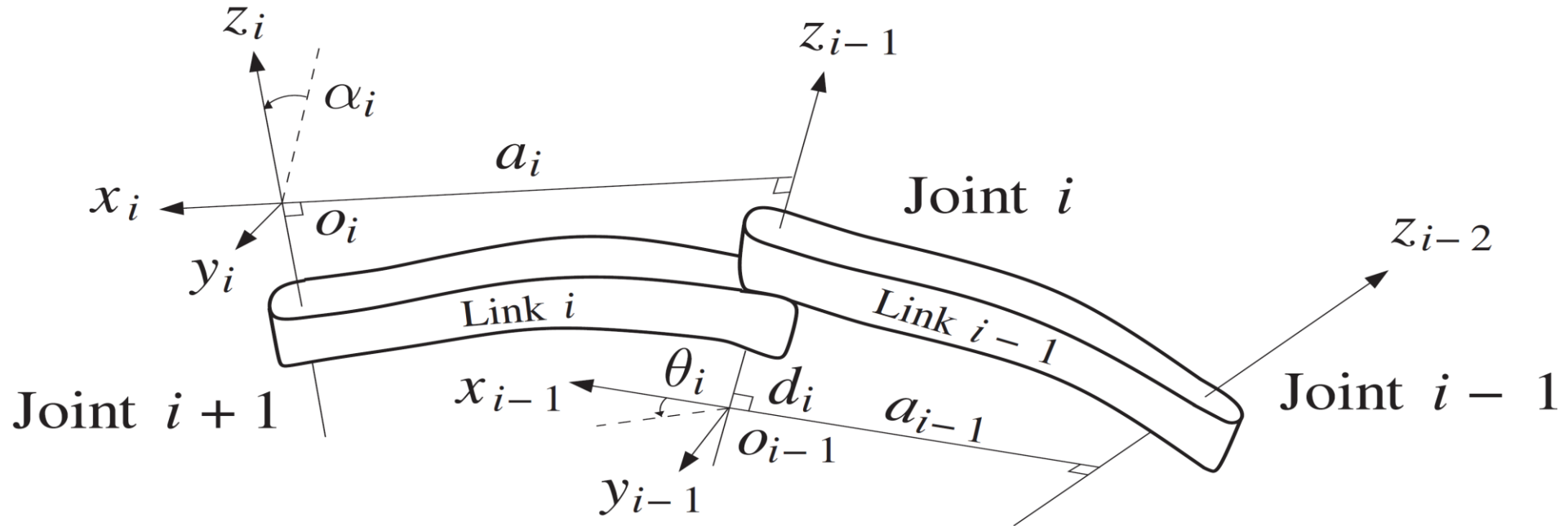
## Positive sense for $\alpha_i$ and $\theta_i$

- $\alpha$  is the angle from  $z_0$  to  $z_1$  measured in a plane normal to  $x_1$  by the right-hand rule.
- $\theta$  is the angle from  $x_0$  to  $x_1$  measured in a plane normal to  $z_0$ .



# The Denavit-Hartenberg Convention

## Assigning the Coordinate Frames



- While frame  $i$  is required to be rigidly attached to link  $i$ , we have considerable freedom in choosing the origin and the coordinate axes of the frame.
- For example, it is not necessary that the origin  $O_i$  of frame  $i$  be placed at the physical end of link  $i$ .
- In fact, it is not even necessary that frame  $i$  be placed within the physical link.
- Frame  $i$  could lie in free space so long as frame  $i$  is rigidly attached to link  $i$ .

# The Denavit-Hartenberg Convention

## *DH Procedure*

**Step 1:** Locate and label the joint axes  $z_0, \dots, z_{n-1}$ .

**Step 2:** Establish the base frame. Set the origin anywhere on the  $z_0$ -axis. The  $x_0$  and  $y_0$  axes are chosen conveniently to form a right-handed frame.

**For**  $i = 1, \dots, n - 1$  perform Steps 3 to 5.

**Step 3:** Locate the origin  $o_i$  where the common normal to  $z_i$  and  $z_{i-1}$  intersects  $z_i$ . If  $z_i$  intersects  $z_{i-1}$  locate  $o_i$  at this intersection. If  $z_i$  and  $z_{i-1}$  are parallel, locate  $o_i$  in any convenient position along  $z_i$ .

**Step 4:** Establish  $x_i$  along the common normal between  $z_{i-1}$  and  $z_i$  through  $o_i$ , or in the direction normal to the  $z_{i-1} - z_i$  plane if  $z_{i-1}$  and  $z_i$  intersect.

**Step 5:** Establish  $y_i$  to complete a right-handed frame.

**Step 6:** Establish the end-effector frame  $o_n x_n y_n z_n$ . Assuming the  $n^{\text{th}}$  joint is revolute, set  $z_n = a$  parallel to  $z_{n-1}$ . Establish the origin  $o_n$  conveniently along  $z_n$ , preferably at the center of the gripper or at the tip of any tool that the manipulator may be carrying. Set  $y_n = s$  in the direction of the gripper closure and set  $x_n = n$  as  $s \times a$ . If the tool is not a simple gripper set  $x_n$  and  $y_n$  conveniently to form a right-handed frame.

# The Denavit-Hartenberg Convention

## *DH Procedure*

**Step 7:** Create a table of DH parameters  $a_i$ ,  $d_i$ ,  $\alpha_i$ ,  $\theta_i$ .

$a_i$  = distance along  $x_i$  from the intersection of the  $x_i$  and  $z_{i-1}$  axes to  $O_i$ .

$d_i$  = distance along  $z_{i-1}$  from  $O_{i-1}$  to the intersection of the  $x_i$  and  $z_{i-1}$  axes. If joint  $i$  is prismatic,  $d_i$  is variable.

$\alpha_i$  = the angle from  $z_{i-1}$  to  $z_i$  measured about  $x_i$ .

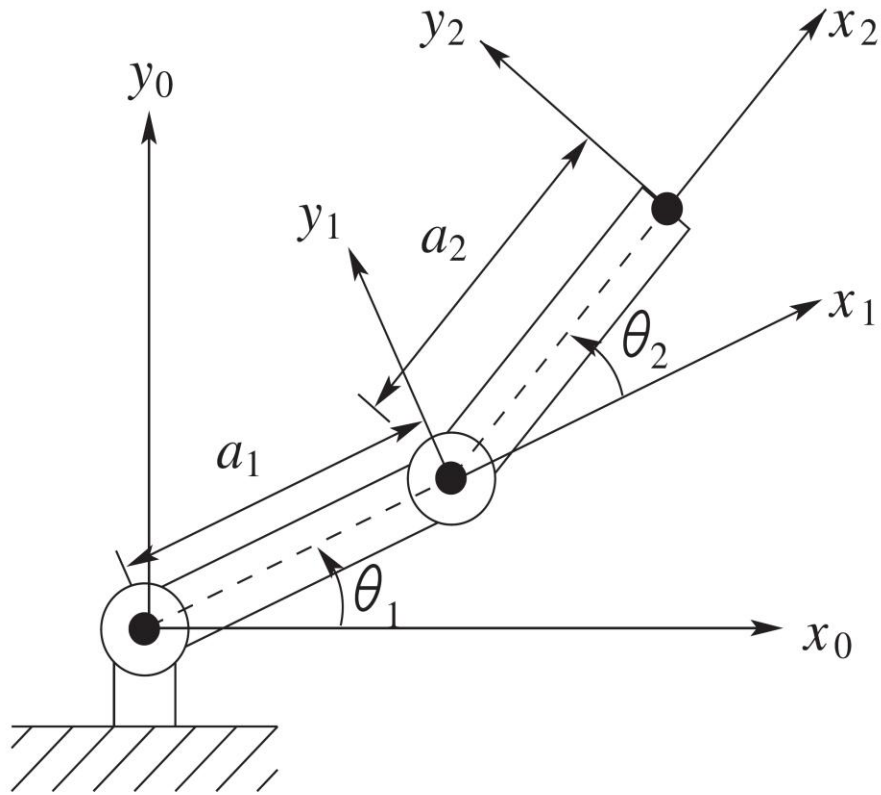
$\theta_i$  = the angle from  $x_{i-1}$  to  $x_i$  measured about  $z_{i-1}$ . If joint  $i$  is revolute,  $\theta_i$  is variable.

**Step 8:** Form the homogeneous transformation matrices  $A_i$  by substituting the above parameters into Equation (3.10).

**Step 9:** Form  $T_n^0 = A_1 \cdots A_n$ . This then gives the position and orientation of the tool frame expressed in base coordinates.

# Examples

## Planar Elbow Manipulator



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1 c_1 \\ s_1 & c_1 & 0 & a_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_2 = \begin{bmatrix} c_2 & -s_2 & 0 & a_2 c_2 \\ s_2 & c_2 & 0 & a_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

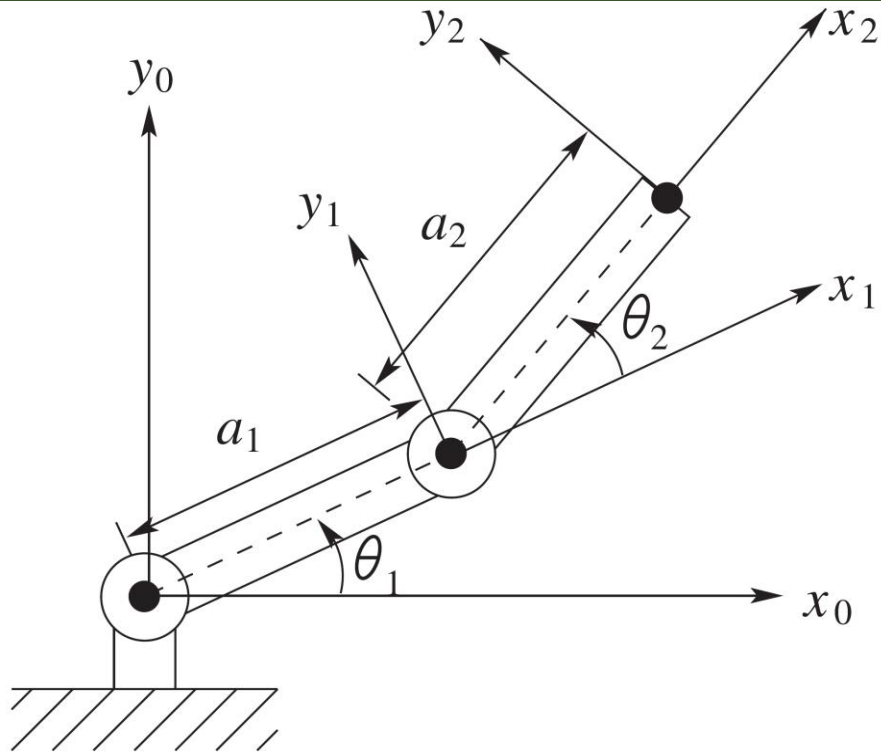
$$T_1^0 = A_1$$

$$T_2^0 = A_1 A_2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1 c_1 + a_2 c_{12} \\ s_{12} & c_{12} & 0 & a_1 s_1 + a_2 s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

- The  $z$ -axes all point out of the page.
- Note that the direction of the  $x_0$  is arbitrary.

# Examples

## Planar Elbow Manipulator



$$T_2^0 = A_1 A_2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & a_1 c_1 + a_2 c_{12} \\ s_{12} & c_{12} & 0 & a_1 s_1 + a_2 s_{12} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$x = a_1 c_1 + a_2 c_{12}$$

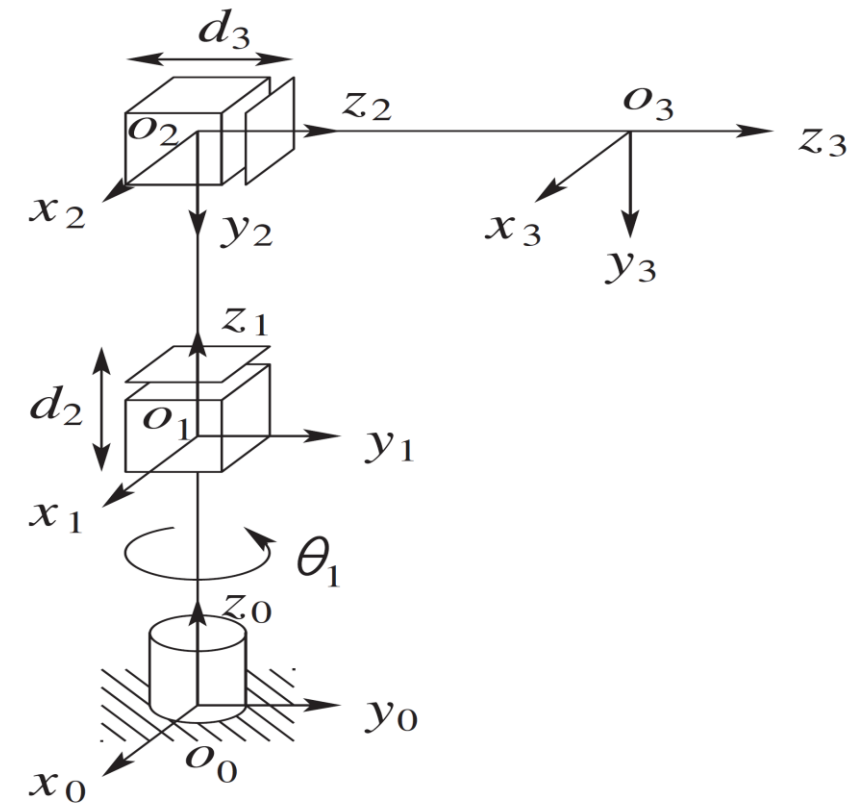
$$y = a_1 s_1 + a_2 s_{12}$$

- Notice that the first two entries of the last column of  $T_2^0$  are the  $x$  and  $y$  components of the origin  $o_2$  in the base frame; that is, are the coordinates of the end effector in the base frame.
- The rotational part of  $T_2^0$  gives the orientation of the frame  $o_2 x_2 y_2 z_2$  relative to the base frame.

# Examples

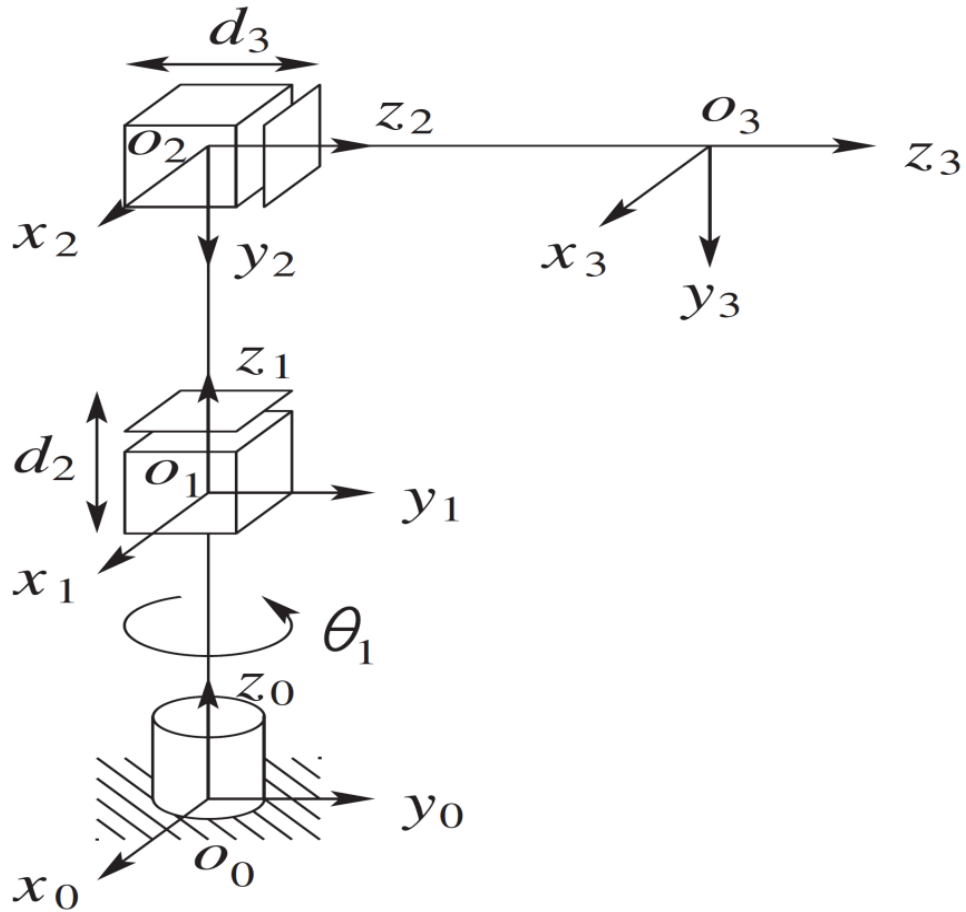
## Three-Link Cylindrical Manipulator

- Note that the placement of the origin  $o_0$  along  $z_0$  and the direction of the  $x_0$  axis are arbitrary.
- $o_0$  could just as well be placed at joint 2.
- Since  $z_0$  and  $z_1$  coincide, the origin  $o_1$  is chosen at joint 2.
- The  $x_1$  axis is parallel to  $x_0$  when  $\theta_1 = 0$  but, of course its direction will change since  $\theta_1$  is variable.
- Since  $z_2$  and  $z_1$  intersect, the origin  $o_2$  is placed at this intersection.
- The direction of  $x_2$  is chosen parallel to  $x_1$  so that  $\theta_2$  is zero.
- Finally, the third frame is chosen at the end of link 3.



# Examples

## Three-Link Cylindrical Manipulator



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	0	0	$d_1$	$\theta_1$
2	0	$-90$	$d_2$	0
3	0	0	$d_3$	0

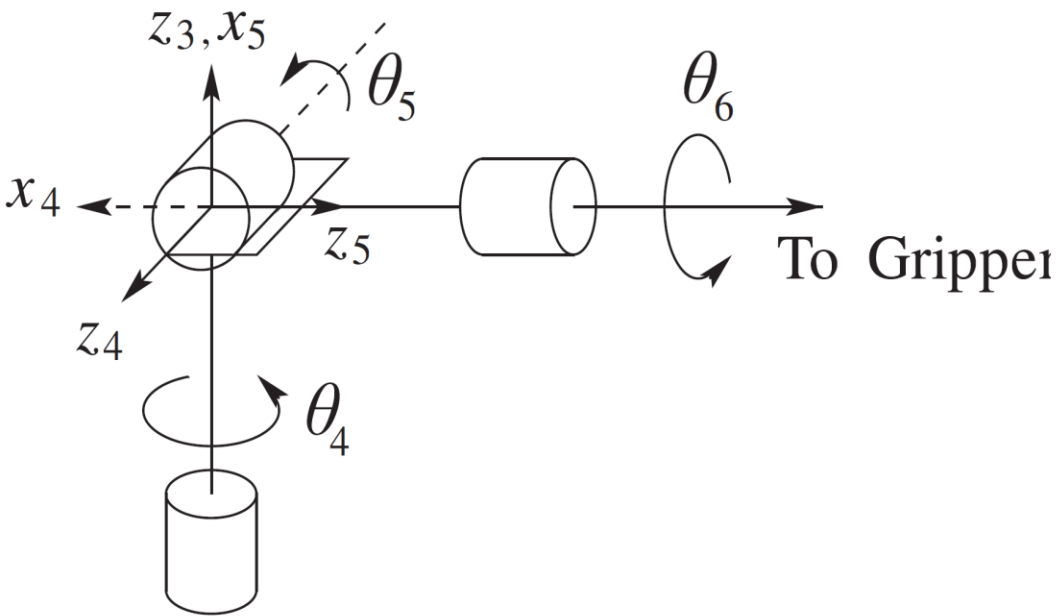
$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_2 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_3^0 = A_1 A_2 A_3 = \begin{bmatrix} c_1 & 0 & -s_1 & -s_1 d_3 \\ s_1 & 0 & c_1 & c_1 d_3 \\ 0 & -1 & 0 & d_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Examples

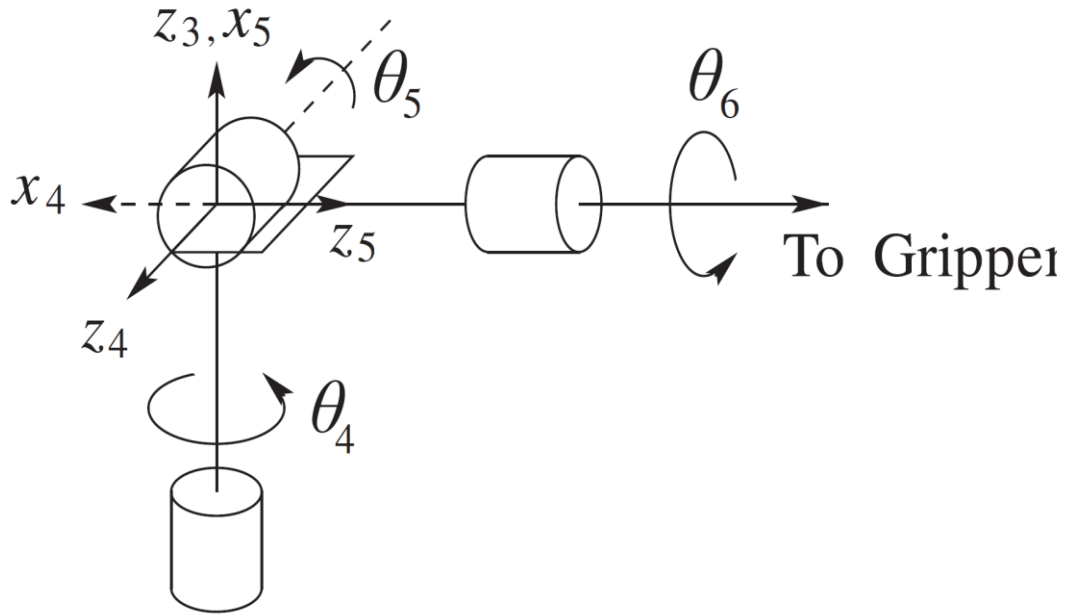
## The Spherical Wrist



- A three-link wrist mechanism for which the joint axes  $z_3, z_4, z_5$  intersect at  $o$ .
- The point  $o$  is called the wrist center.
- $\theta_4; \theta_5; \theta_6$  can be identified as the Euler angles  $\varphi, \theta$  and  $\psi$  with respect to the coordinate frame  $o_3x_3y_3z_3$ .

# Examples

## The Spherical Wrist



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
4	0	-90	0	$\theta_4$
5	0	90	0	$\theta_5$
6	0	0	$d_6$	$\theta_6$

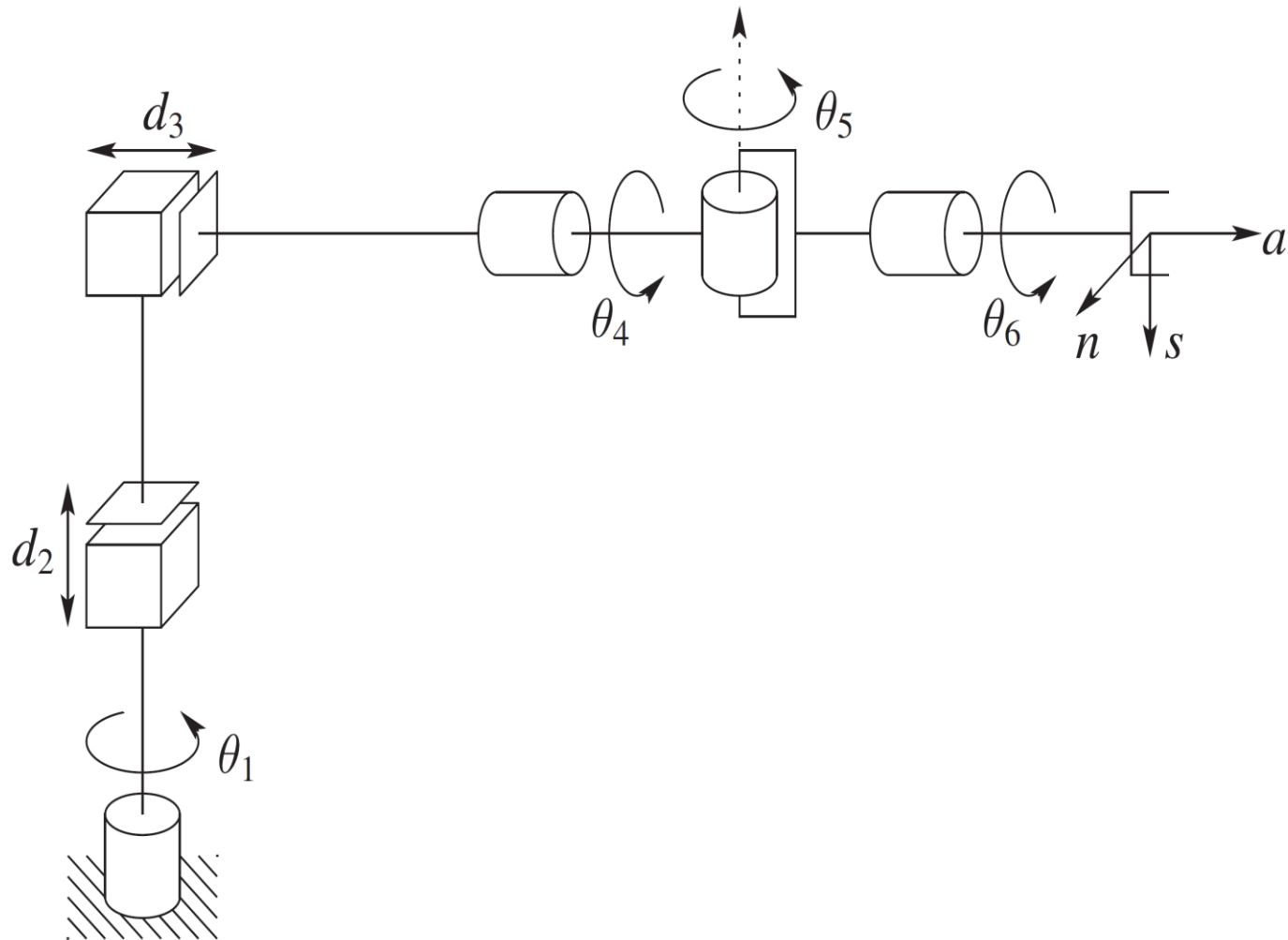
$$A_4 = \begin{bmatrix} c_4 & 0 & -s_4 & 0 \\ s_4 & 0 & c_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_5 = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_6 = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{aligned} T_6^3 &= A_4 A_5 A_6 \\ &= \begin{bmatrix} R_6^3 & o_6^3 \\ 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & c_4 s_5 & c_4 s_5 d_6 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & s_4 s_5 & s_4 s_5 d_6 \\ -s_5 c_6 & s_5 s_6 & c_5 & c_5 d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

# Examples

## Cylindrical Manipulator with Spherical Wrist



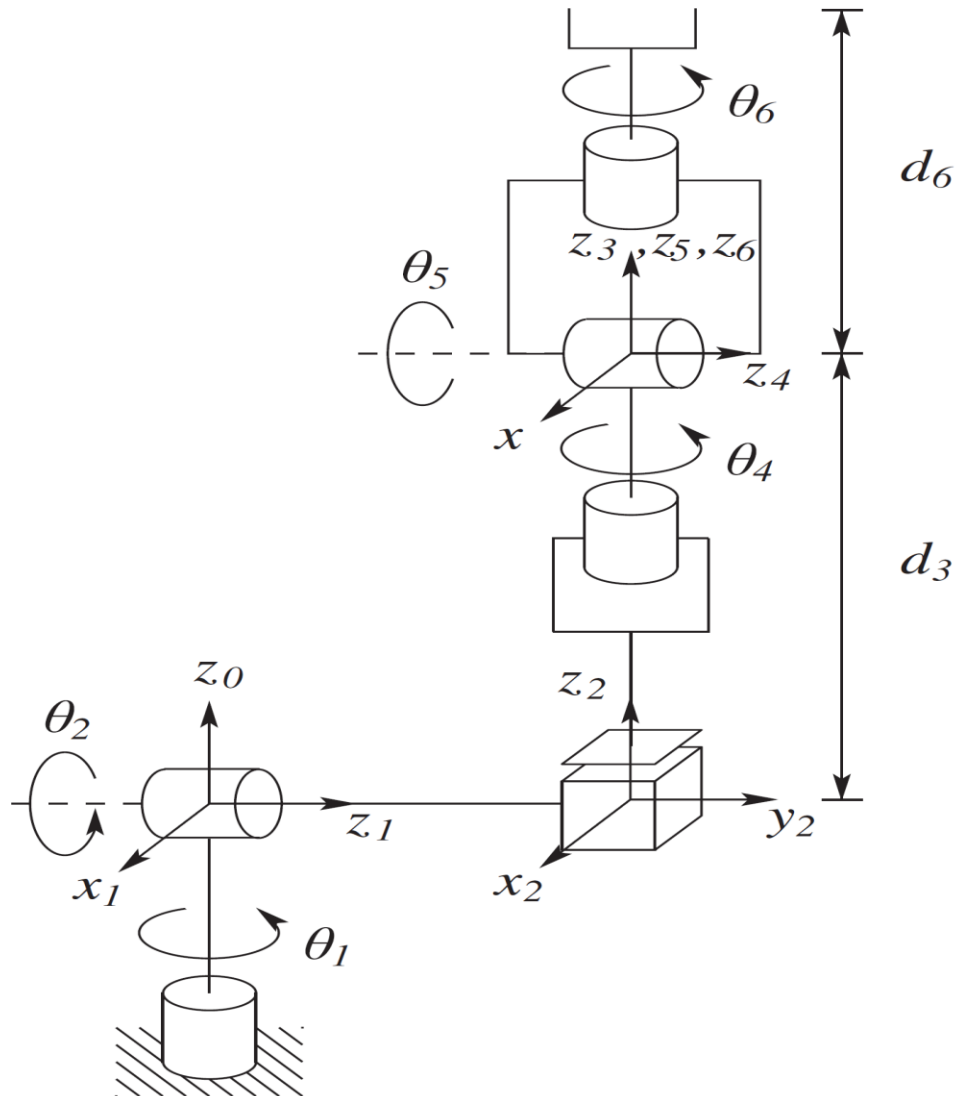
$$T_6^0 = T_3^0 T_6^3$$

From Example 2

From Example 3

# Examples

## Stanford Manipulator



Link	$d_i$	$a_i$	$\alpha_i$	$\theta_i$
1	0	0	-90	$\theta_1$
2	$d_2$	0	+90	$\theta_2$
3	$d_3$	0	0	0
4	0	0	-90	$\theta_4$
5	0	0	+90	$\theta_5$
6	$d_6$	0	0	$\theta_6$

$$T_6^0 = A_1 \cdots A_6 = \begin{bmatrix} r_{11} & r_{12} & r_{13} & d_x \\ r_{21} & r_{22} & r_{23} & d_y \\ r_{31} & r_{32} & r_{33} & d_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_1 = \begin{bmatrix} c_1 & 0 & -s_1 & 0 \\ s_1 & 0 & c_1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} c_2 & 0 & s_2 & 0 \\ s_2 & 0 & -c_2 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

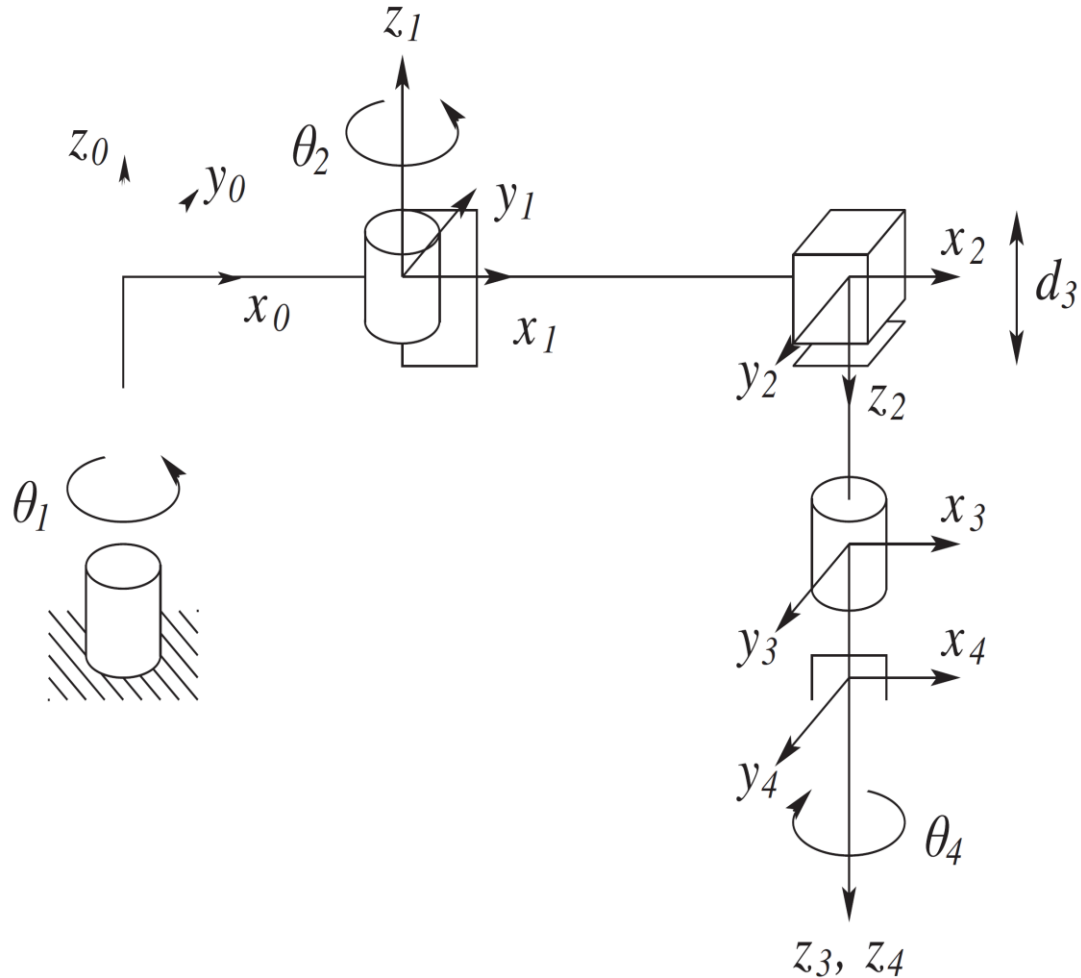
$$A_4 = \begin{bmatrix} c_4 & 0 & -s_4 & 0 \\ s_4 & 0 & c_4 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_5 = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_6 = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Examples

## SCARA Manipulator



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1$
2	$a_2$	180	0	$\theta_2$
3	0	0	$d_3$	0
4	0	0	$d_4$	$\theta_4$

$$T_4^0 = A_1 \cdots A_4 = \begin{bmatrix} c_{12}c_4 + s_{12}s_4 & -c_{12}s_4 + s_{12}c_4 & 0 & a_1c_1 + a_2c_{12} \\ s_{12}c_4 - c_{12}s_4 & -s_{12}s_4 - c_{12}c_4 & 0 & a_1s_1 + a_2s_{12} \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_1 = \begin{bmatrix} c_1 & -s_1 & 0 & a_1c_1 \\ s_1 & c_1 & 0 & a_1s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_2 = \begin{bmatrix} c_2 & s_2 & 0 & a_2c_2 \\ s_2 & -c_2 & 0 & a_2s_2 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_3 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad A_4 = \begin{bmatrix} c_4 & -s_4 & 0 & 0 \\ s_4 & c_4 & 0 & 0 \\ 0 & 0 & 1 & d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# MATLAB: Robotics System Toolbox

## Forward Kinematics

### First Method

```
theta=deg2rad(60); d=0;  
alpha=deg2rad(0); a=1;  
Rot_z=axang2tform([0 0 1 theta]);  
Trans_z=trvec2tform([0 0 d]);  
Rot_x=axang2tform([1 0 0 alpha]);  
Trans_x=trvec2tform([a 0 0]);  
A=Rot_z*Trans_z*Trans_x*Rot_x;
```

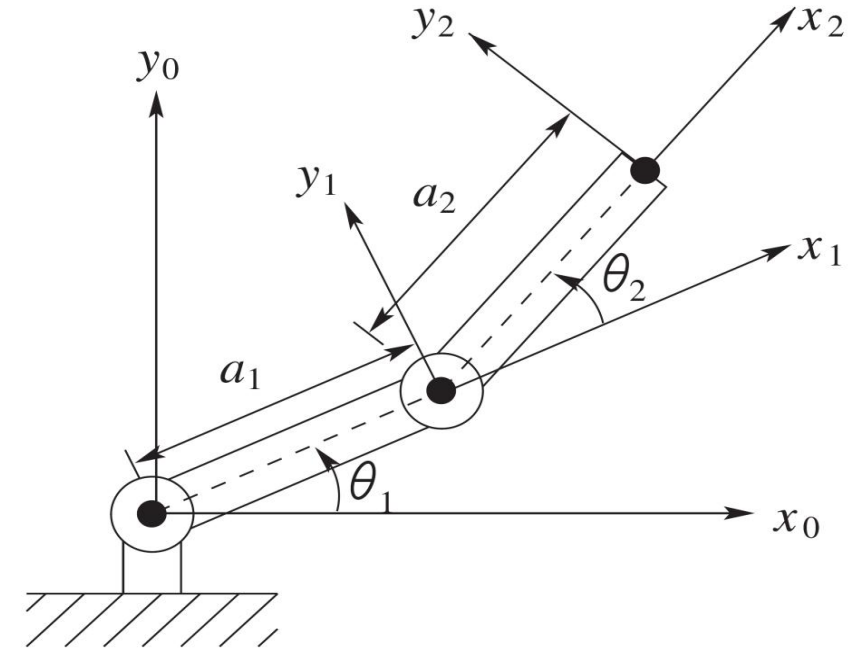
$$\begin{aligned} A_i &= \text{Rot}_{z,\theta_i} \text{Trans}_{z,d_i} \text{Trans}_{x,a_i} \text{Rot}_{x,\alpha_i} \\ &= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i} & 0 & 0 \\ s_{\theta_i} & c_{\theta_i} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ &\quad \times \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & c_{\alpha_i} & -s_{\alpha_i} & 0 \\ 0 & s_{\alpha_i} & c_{\alpha_i} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} c_{\theta_i} & -s_{\theta_i} c_{\alpha_i} & s_{\theta_i} s_{\alpha_i} & a_i c_{\theta_i} \\ s_{\theta_i} & c_{\theta_i} c_{\alpha_i} & -c_{\theta_i} s_{\alpha_i} & a_i s_{\theta_i} \\ 0 & s_{\alpha_i} & c_{\alpha_i} & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

# MATLAB: Robotics System Toolbox

## Forward Kinematics

*Example*

```
theta1=deg2rad(60); d1=0;  
alpha1=deg2rad(0); a1=1;  
Rot_z1=axang2tform([0 0 1 theta1]);  
Trans_z1=trvec2tform([0 0 d1]);  
Rot_x1=axang2tform([1 0 0 alpha1]);  
Trans_x1=trvec2tform([a1 0 0]);  
A1=Rot_z1*Trans_z1*Trans_x1*Rot_x1;
```



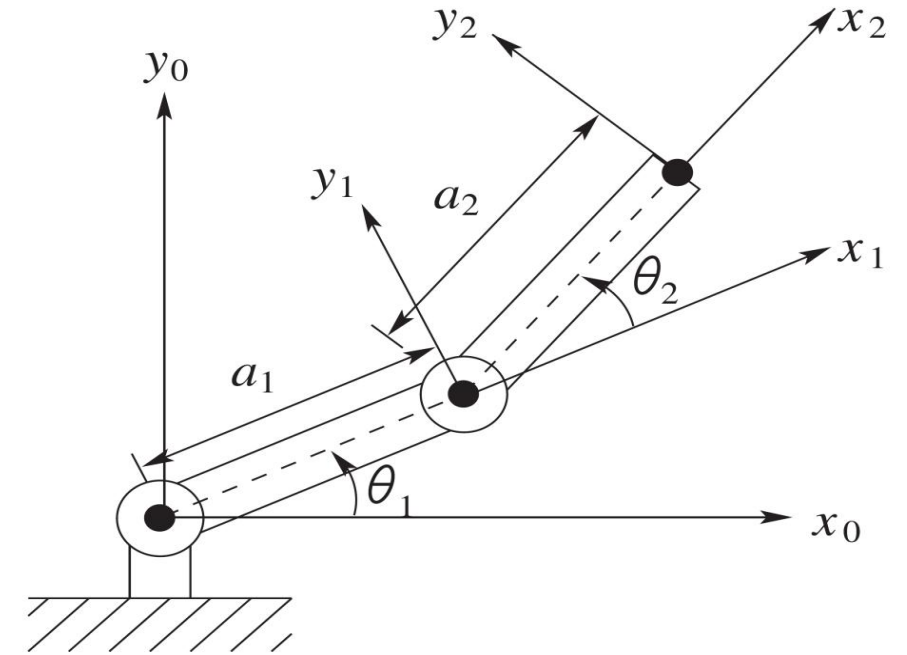
Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$

# MATLAB: Robotics System Toolbox

## Forward Kinematics

### Example

```
theta2=deg2rad(30); d2=0;  
alpha2=deg2rad(0); a2=0.5;  
Rot_z2=axang2tform([0 0 1 theta2]);  
Trans_z2=trvec2tform([0 0 d2]);  
Rot_x2=axang2tform([1 0 0 alpha2]);  
Trans_x2=trvec2tform([a2 0 0]);  
A2=Rot_z2*Trans_z2*Trans_x2*Rot_x2;  
T=A1*A2;
```



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$

# MATLAB: Robotics System Toolbox

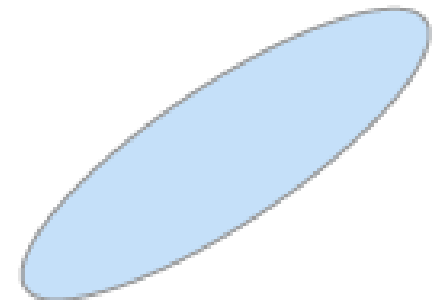
## Rigid Body Tree Robot Model

The rigid body tree model is a representation of a robot structure. You can use it to represent robots such as manipulators or other kinematic trees. Use [rigidBodyTree](#) objects to create these models.

### Rigid Body Tree Components

**Base:** Every rigid body tree has a base. The base defines the world coordinate frame and is the first attachment point for a rigid body.

**Rigid Body:** The rigid body is the basic building block of rigid body tree model and is created using [rigidBody](#). A rigid body, sometimes called a link, represents a solid body that cannot deform. The distance between any two points on a single rigid body remains constant. Each rigid body has a coordinate frame associated with them and contains a [rigidBodyJoint](#) object.

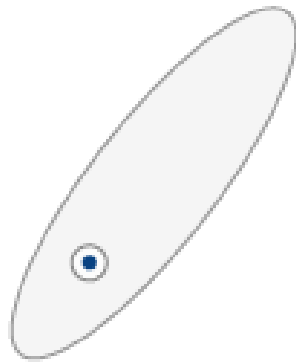


# MATLAB: Robotics System Toolbox

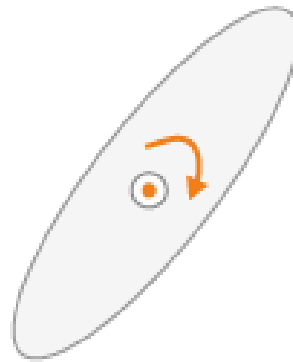
## Rigid Body Tree Robot Model

**Joint:** Each rigid body has one joint, which defines the motion of that rigid body relative to its parent. It is the attachment point that connects two rigid bodies in a robot model.

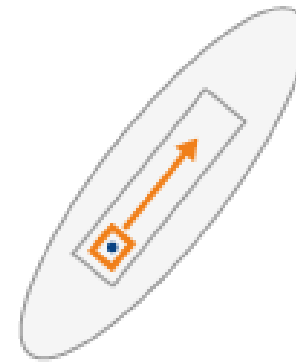
The [rigidBodyJoint](#) object supports fixed, revolute, and prismatic joints.



*Fixed*



*Revolute*



*Prismatic*

# MATLAB: Robotics System Toolbox

## Rigid Body Tree Robot Model

### *setFixedTransform*

Set fixed transform properties of joint

#### *Syntax*

*setFixedTransform(jointObj,tform)*

*setFixedTransform(jointObj,dhparams,"dh")*

- DH parameters are given in the order [a alpha d theta].
- For revolute joints, the theta input is ignored when specifying the fixed transformation between joints because that angle is dependent on the joint configuration. For prismatic joints, the d input is ignored

# MATLAB: Robotics System Toolbox

## Rigid Body Tree Robot Model

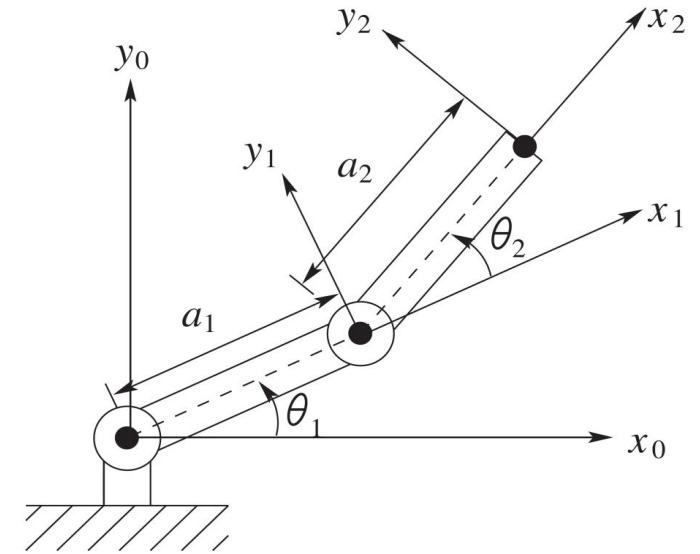
<b>importrobot</b>	Import rigid body tree model from URDF file, text, or Simscape Multibody model
<b>loadrobot</b>	Load rigid body tree robot model
<b>rigidBodyTree</b>	Create tree-structured robot
<b>rigidBody</b>	Create a rigid body
<b>rigidBodyJoint</b>	Create a joint
<b>interactiveRigidBodyTree</b>	Interact with rigid body tree robot models

# MATLAB: Robotics System Toolbox

## Forward Kinematics

### Second Method

```
robot = rigidBodyTree;  
body1 = rigidBody('body1');  
body2 = rigidBody('body2');  
bodyEndEffector = rigidBody('endeffector');  
jnt1 = rigidBodyJoint('jnt1','revolute');  
jnt2 = rigidBodyJoint('jnt2','revolute');  
jnt1.HomePosition = deg2rad(0);  
jnt2.HomePosition = deg2rad(0);  
dh1=[1 0 0 deg2rad(60)];  
dh2=[0.5 0 0 deg2rad(30)];  
setFixedTransform(jnt1,dh1,'dh');  
setFixedTransform(jnt2,dh2,'dh');  
body1.Joint = jnt1;  
body2.Joint = jnt2;
```



Link	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$a_1$	0	0	$\theta_1$
2	$a_2$	0	0	$\theta_2$

# MATLAB: Robotics System Toolbox

## Forward Kinematics

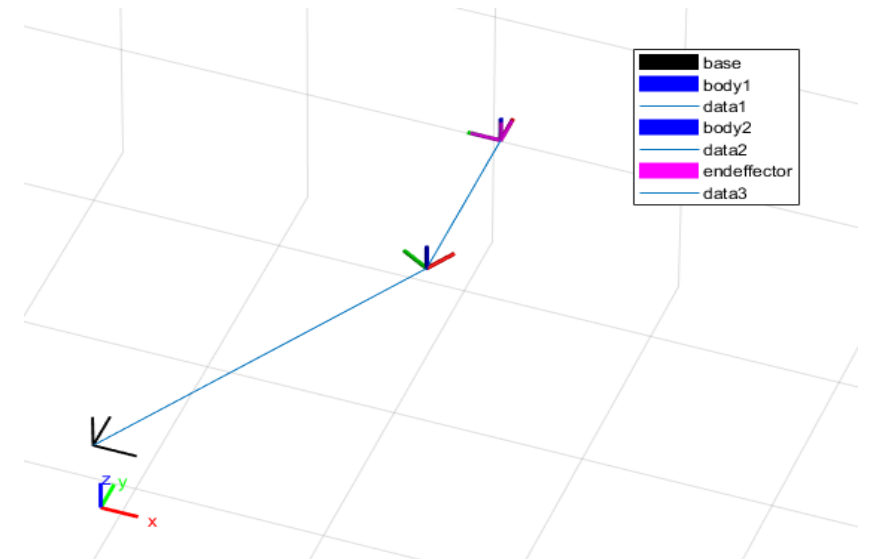
### Second Method

```
addBody(robot,body1,'base');  
addBody(robot,body2,'body1');  
addBody(robot,bodyEndEffector,'body2');  
config = homeConfiguration(robot)  
config(1).JointPosition = deg2rad(60)  
config(2).JointPosition = deg2rad(30)  
T = getTransform(robot,config,'endeffector','base')  
showdetails(robot)  
show(robot,config)
```

### Result

T =

0.0000	-1.0000	0	0.5000
1.0000	0.0000	0	1.3660
0	0	1.0000	0
0	0	0	1.0000



*Thank You*

*Any Questions ??*