

Mechatronics Engineering Department
Faculty of Engineering
Ain Shams University



MCT344/MCT342/CSE373/CSE471: Robotics
Lecture 13: Robot Control II

Presented by : Prof. Mohammed Ibrahim Awad

Robotic Mechanical Components



<https://www.youtube.com/shorts/uIpYJRRgK9U>

<https://www.youtube.com/shorts/80aE5XF4T2M>

<https://www.youtube.com/shorts/NtucDVCYnaw>

Joint space control

Consideration #2

The diagonal of the matrix $\mathbf{M}(\mathbf{q})$ is composed by two kinds of elements

- Inertia terms that do not depend on the robot's configuration
- Terms that depend on the robot's configuration.

Therefore:

$$\mathbf{M}(\mathbf{q}) = \bar{\mathbf{M}} + \Delta\mathbf{M}(\mathbf{q})$$

where $\bar{\mathbf{M}}$ is a diagonal matrix with constant elements (i.e. the mean values of the joints inertia). From the robot dynamic model it follows

$$\boldsymbol{\tau}_m = (\mathbf{K}_r^{-1} \bar{\mathbf{M}} \mathbf{K}_r^{-1}) \ddot{\mathbf{q}}_m + \mathbf{D}_m \dot{\mathbf{q}}_m + \mathbf{d}$$

where

$$\mathbf{D}_m = \mathbf{K}_r^{-1} \mathbf{D} \mathbf{K}_r^{-1}$$

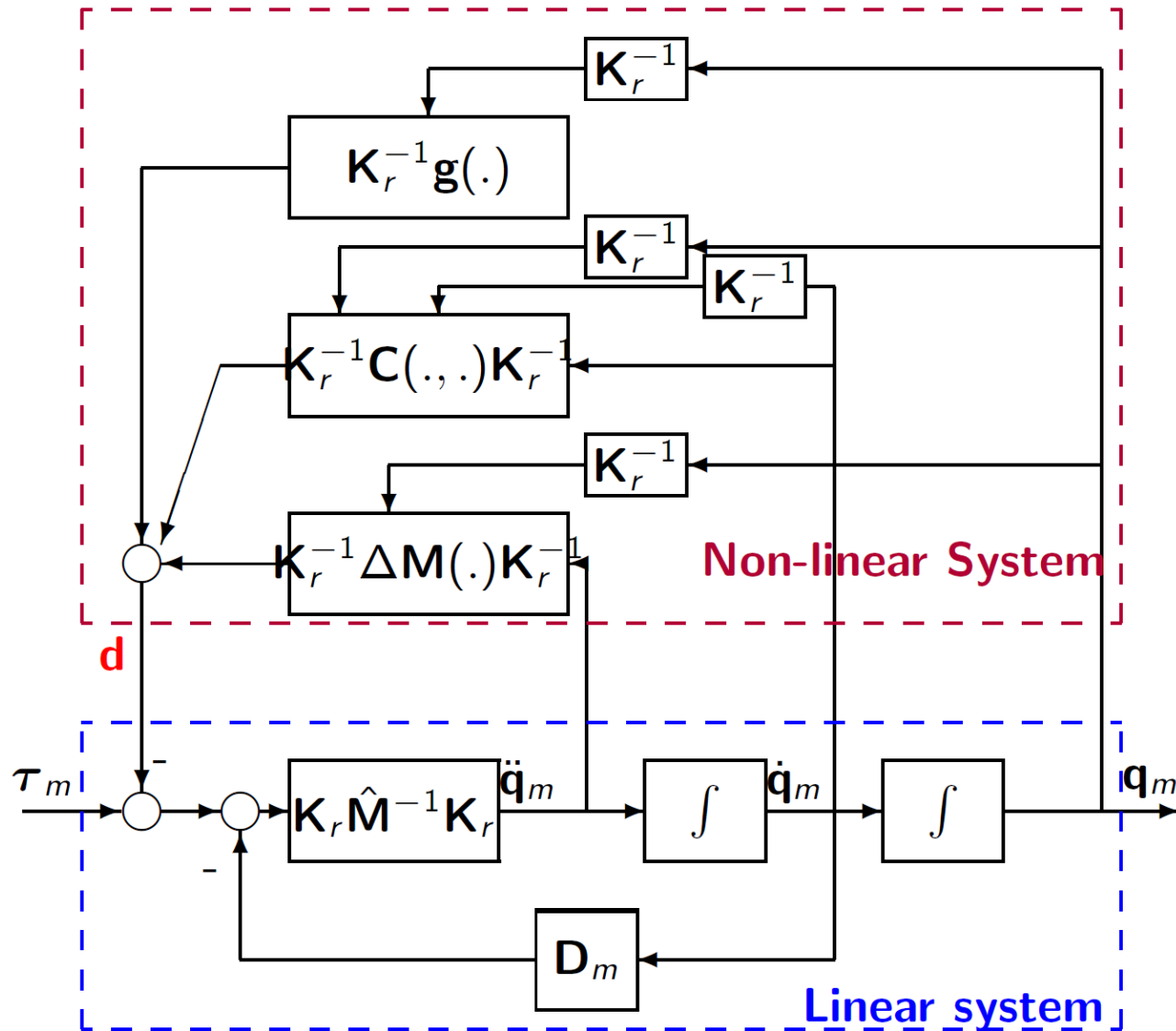
is the matrix collecting the motors friction coefficients, and

$$\mathbf{d} = (\mathbf{K}_r^{-1} \Delta\mathbf{M}(\mathbf{q}) \mathbf{K}_r^{-1}) \ddot{\mathbf{q}}_m + (\mathbf{K}_r^{-1} \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) \mathbf{K}_r^{-1}) \dot{\mathbf{q}}_m + \mathbf{K}_r^{-1} \mathbf{g}(\mathbf{q})$$

is a term that can be considered as a disturbance.

Joint space control

$$\ddot{\mathbf{q}}_m = \mathbf{K}_r \hat{\mathbf{M}}^{-1} \mathbf{K}_r (\boldsymbol{\tau}_m - \mathbf{D}_m \dot{\mathbf{q}}_m - \mathbf{d}) \implies$$



A manipulator (+ the actuation system) can be regarded as the composition of:

- a system with input $\ddot{\mathbf{q}}_m, \dot{\mathbf{q}}_m, \mathbf{q}_m$ and output \mathbf{d} , *non linear and with couplings*
- a system with input $\boldsymbol{\tau}_m$ and output \mathbf{q}_m , *linear and decoupled*

Centralized control

Dynamic model of a manipulator:

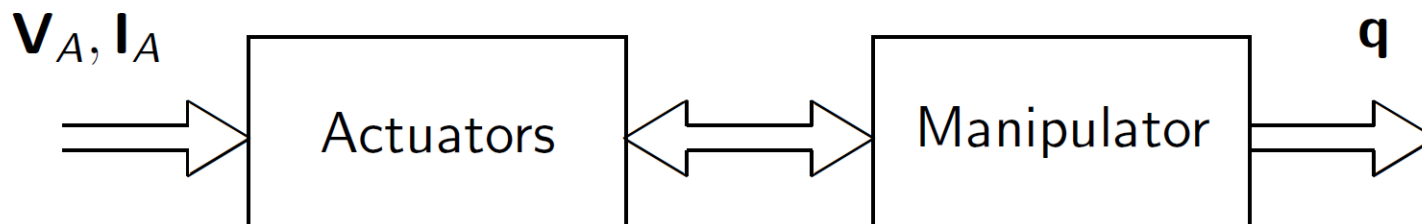
$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{D}_v\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \boldsymbol{\tau}$$

Actuators and gearboxes may be described by:

$$\begin{aligned}\mathbf{K}_r\mathbf{q} &= \mathbf{q}_m \\ \mathbf{v}_A &= \mathbf{G}_v\mathbf{v}_c \\ \mathbf{v}_A &= \mathbf{R}_A\mathbf{I}_A + \mathbf{K}_v\dot{\mathbf{q}}_m \\ \boldsymbol{\tau}_m &= \mathbf{K}_t\mathbf{I}_A = \mathbf{K}_r^{-1}\boldsymbol{\tau}\end{aligned}$$

where \mathbf{K}_r is the matrix with the reduction coefficients; \mathbf{G}_v the gain of the motor drives; \mathbf{R}_A the armature resistances; $\mathbf{K}_v, \mathbf{K}_t$ the electro-mechanic constants of the motors.

Consider the manipulator as a MIMO system with n input and n output.



Centralized control

Voltage control mode:

$$\begin{aligned}\mathbf{I}_A &= \mathbf{R}_A^{-1}(\mathbf{v}_A - \mathbf{K}_v \dot{\mathbf{q}}_m) \\ &= \mathbf{R}_A^{-1} \mathbf{G}_v \mathbf{v}_c - \mathbf{R}_A^{-1} \mathbf{K}_v \mathbf{K}_r \dot{\mathbf{q}}\end{aligned}$$

$$\begin{aligned}\boldsymbol{\tau} &= \mathbf{K}_r \mathbf{K}_t \mathbf{I}_A \\ &= \mathbf{K}_r \mathbf{K}_t \mathbf{R}_A^{-1} \mathbf{G}_v \mathbf{v}_c - \mathbf{K}_r \mathbf{K}_t \mathbf{R}_A^{-1} \mathbf{K}_v \mathbf{K}_r \dot{\mathbf{q}}\end{aligned}$$

Thus, the robot dynamic equation becomes:

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{D}\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \mathbf{u}$$

where

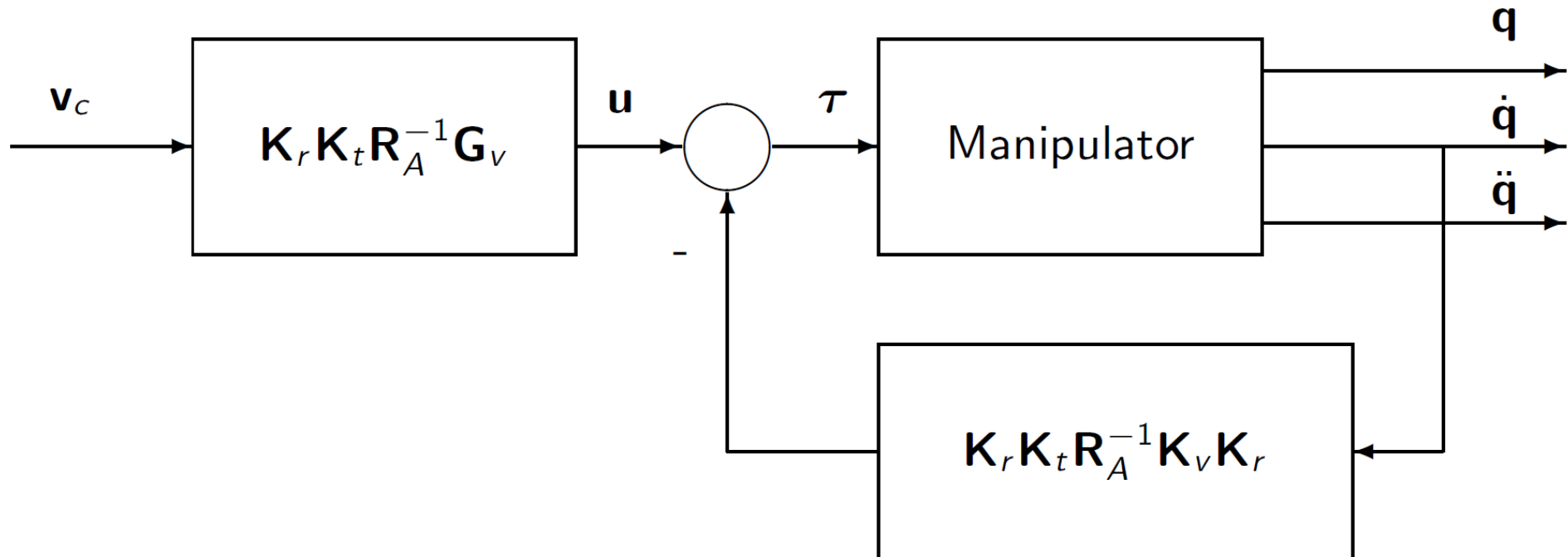
$$\begin{aligned}\mathbf{D} &= \mathbf{D}_v + \mathbf{K}_r \mathbf{K}_t \mathbf{R}_A^{-1} \mathbf{K}_v \mathbf{K}_r && \implies && \text{diagonal matrix with friction terms} \\ \mathbf{u} &= \mathbf{K}_r \mathbf{K}_t \mathbf{R}_A^{-1} \mathbf{G}_v \mathbf{v}_c && \implies && \text{control input}\end{aligned}$$

Centralized control

Manipulator dynamic model:

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{D}\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \mathbf{u}$$

The torque $\boldsymbol{\tau}$ (real input generating the motion of the manipulator) is not equal to \mathbf{u} (algebraically related to \mathbf{v}_c) because of the counter-electromotive force proportional to the joints velocity $\dot{\mathbf{q}}$.



Centralized control

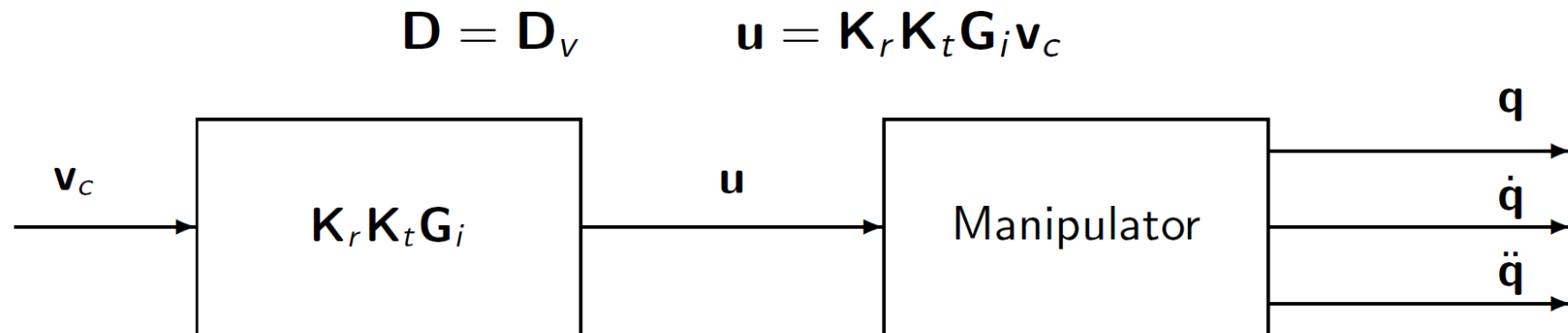
Torque control mode: With the voltage-control mode, it is not possible to directly provide to the joints the exact torques needed to move the robot (complex computation should be introduced to compensate for the velocity-dependent terms). It is preferable to use for the motor a current-control modality: the actuator acts as a torque generator.

$$\mathbf{I}_A = \mathbf{G}_i \mathbf{v}_c$$

It follows:

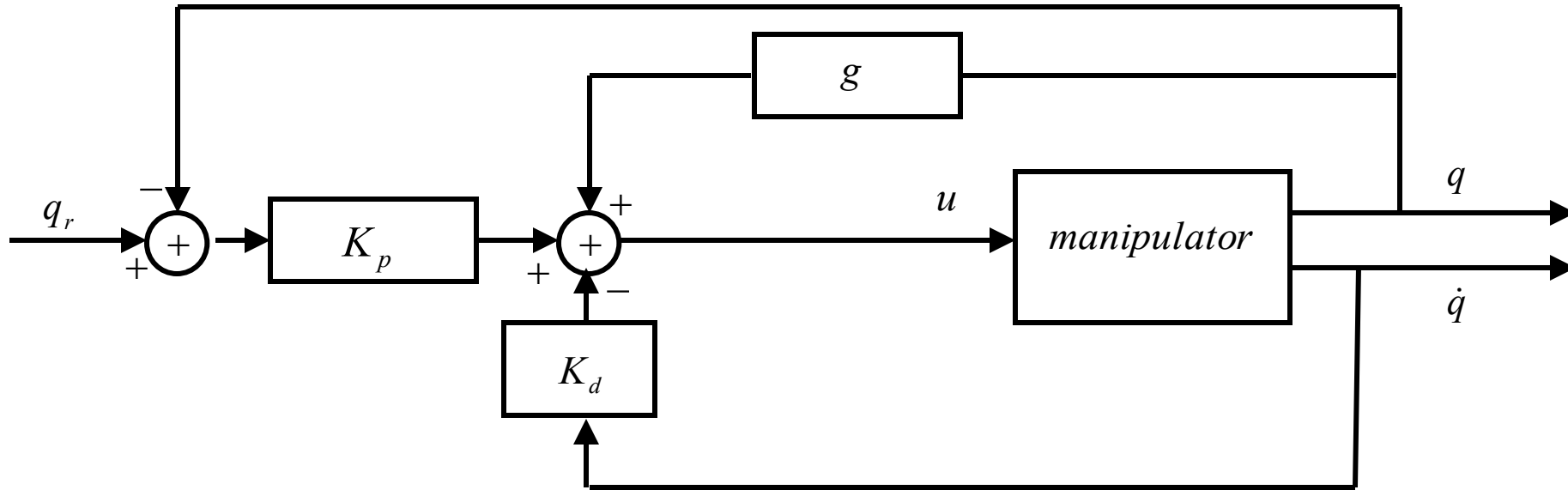
$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{D}\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \mathbf{u}$$

where



Compensating for gravity

PD rate feedback control (notice no integrator):



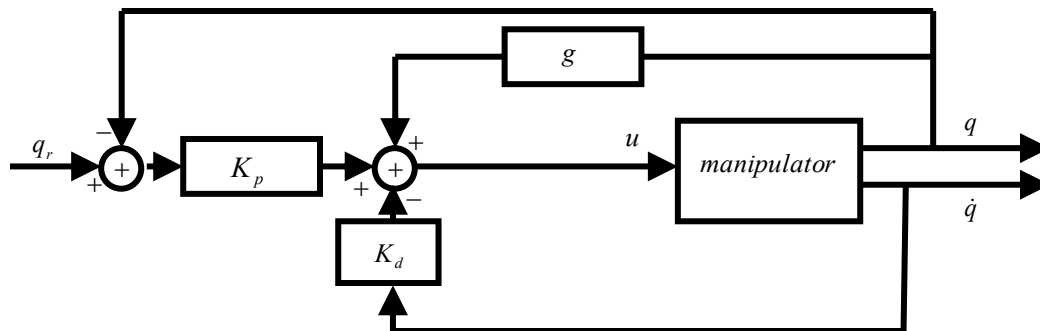
$$u = g(q) + K_p(q_d - q) - K_d\dot{q} \quad \text{where} \quad g = \sum_{i=1}^n m_i g^T \frac{\partial p_i}{\partial q_k}$$

$$M(q)\ddot{q}_i + C(q, \dot{q})\dot{q}_i + g(q) = u$$

$$M(q)\ddot{q}_i + C(q, \dot{q})\dot{q}_i + g(q) = g(q) + K_p(q_d - q) - K_d\dot{q}$$

$$\text{At equilibrium: } K_p(q_d - q) = 0$$

Compensating for gravity



$$u = g(q) + K_p (q_d - q) - K_d \dot{q}$$

$$M(q)\ddot{q}_i + C(q, \dot{q})\dot{q}_i + g(q) = u$$

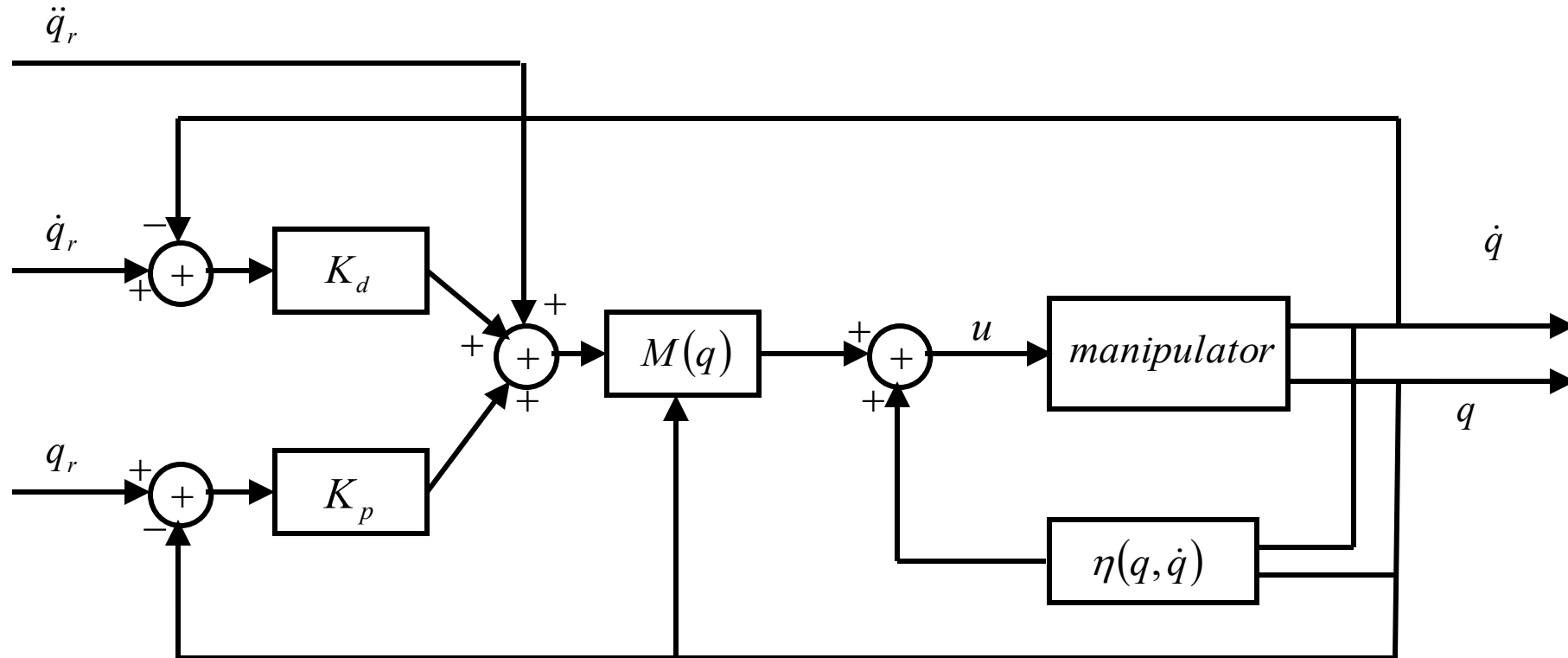
$$M(q)\ddot{q}_i + C(q, \dot{q})\dot{q}_i + g(q) = g(q) + K_p (q_d - q) - K_d \dot{q}$$

Resulting equation of motion:

$$M(q)\ddot{q}_i + (C(q, \dot{q}) - K_d)\dot{q}_i + K_p (q_d - q) = 0$$

At equilibrium: $K_p (q_d - q) = 0$

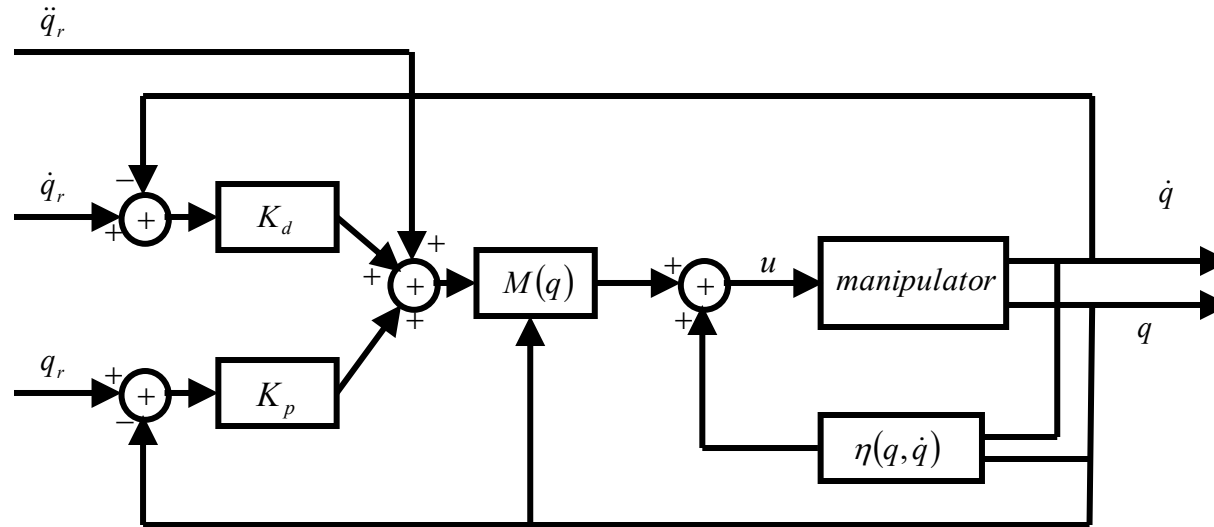
Inverse dynamics control



$$M(q)\ddot{q}_i + C(q, \dot{q})\dot{q}_i + g(q) = u$$

$$u = M(q)\left[\ddot{q}_d + K_d(\dot{q}_d - \dot{q}) + K_p(q_d - q)\right] + C(q, \dot{q})\dot{q}_i + g(q)$$

Inverse dynamics control



$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = u$$

$$u = M(q)\left[\ddot{q}_d + K_d(\dot{q}_d - \dot{q}) + K_p(q_d - q)\right] + C(q, \dot{q})\dot{q} + g(q)$$

$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = M(q)\left[\ddot{q}_d + K_d(\dot{q}_d - \dot{q}) + K_p(q_d - q)\right] + C(q, \dot{q})\dot{q} + g(q)$$

$$(\ddot{q}_d - \ddot{q}) + K_d(\dot{q}_d - \dot{q}) + K_p(q_d - q) = 0$$

Force and Interaction Control

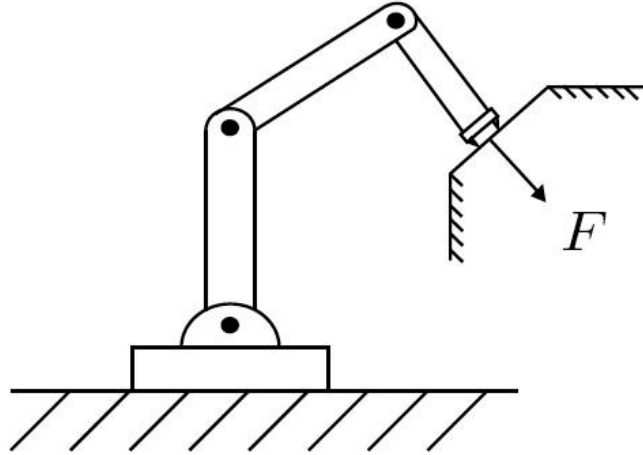


Figure 9.2: Robot end effector in contact with a rigid surface.

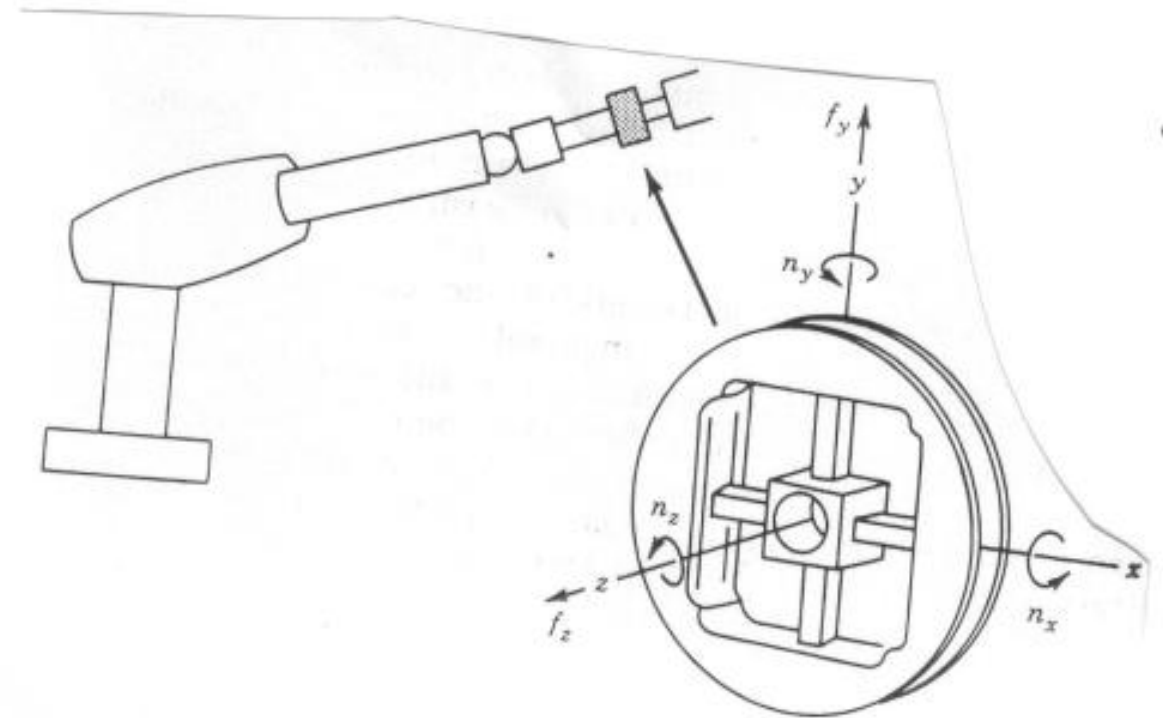
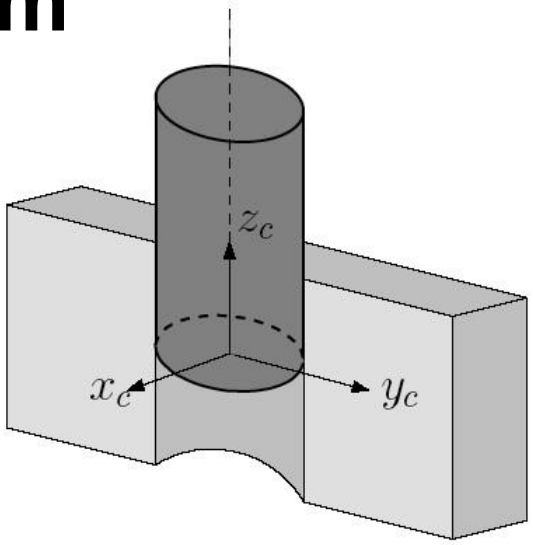
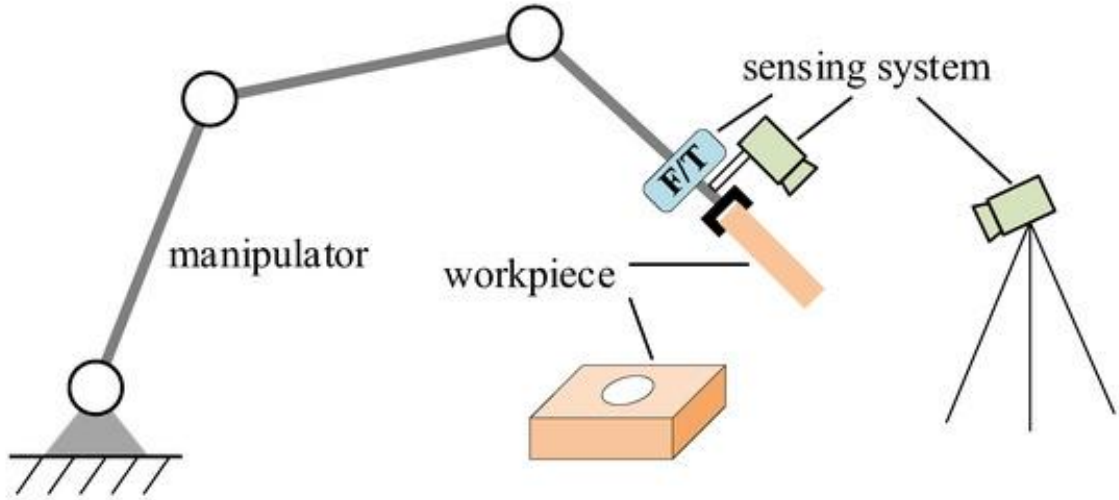


Fig. 9.1 A Wrist Force Sensor.

Peg and Hole Assembly Problem



Natural Constraints	Artificial Constraints
$v_x = 0$	$f_x = 0$
$v_y = 0$	$f_y = 0$
$f_z = 0$	$v_z = v_d$
$\omega_x = 0$	$n_x = 0$
$\omega_y = 0$	$n_y = 0$
$n_z = 0$	$\omega_z = 0$

Figure 9.3: Inserting a peg into a hole.



Peg and Hole Assembly Problem



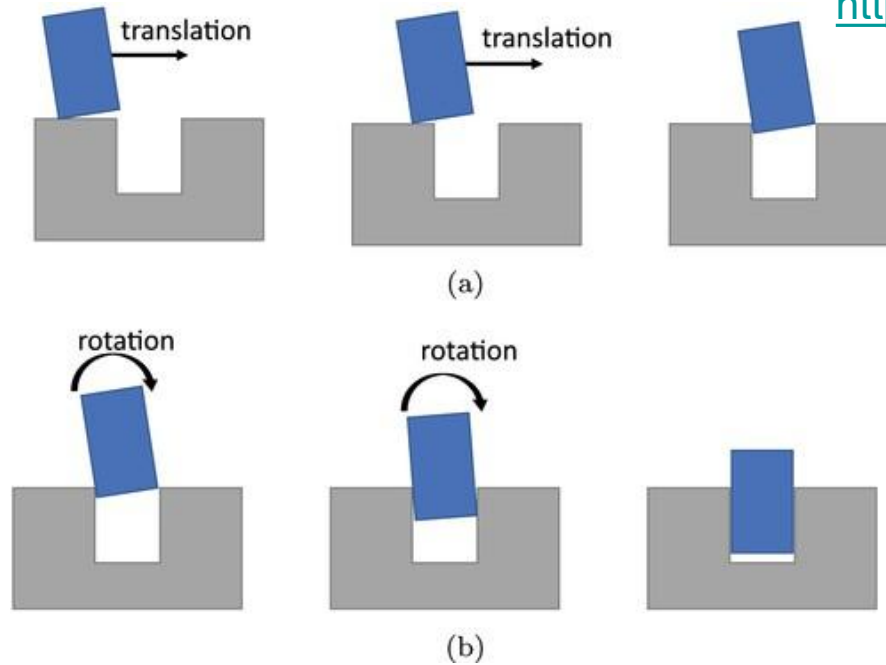
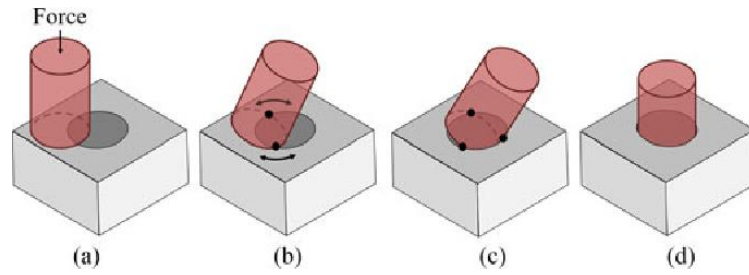
Performance Analysis of a Robotics Vision System and Localization
using Fusion of Vision and Force/Torque Data for Robotic Assembly

Riby Abraham Bobby and Karam Almaghout

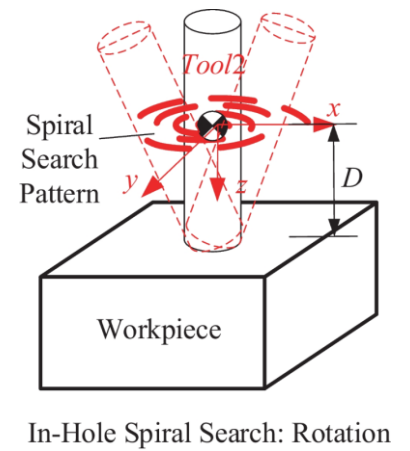
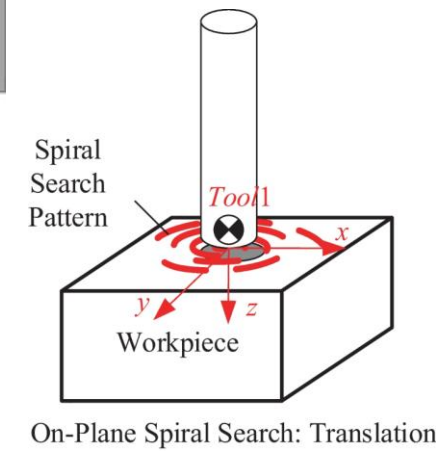
Innopolis University

2021

Hole search strategy



<https://www.youtube.com/watch?v=g2un1ieA7IM>



<https://www.youtube.com/shorts/stHFbmHeJ9Q>

Peg-In-Hole Using 3D Workpiece Reconstruction and CNN-Based Hole Detection

2020 IEEE/RSJ

International Conference on
Intelligent Robots and Systems(IROS)

October 25-29, 2020 Las Vegas, NV, USA



Theme: Consumer Robotics and Our Future

Peg-in-Hole Using 3D Workpiece Reconstruction and CNN-based Hole Detection

**M. Nigro, M. Sileo, F. Pierri,
K. Genovese, D.D. Bloisi, F. Caccavale**



University of Basilicata, 85100, Potenza, Italy

www.unibas.it/automatica

<http://web.unibas.it/bloisi/>

<https://www.youtube.com/watch?v=I7Ujj0Y81g>

Robot Manipulation: Meta Learning and Adaptive Control

A Framework for Robot Manipulation: Skill Formalism, Meta Learning and Adaptive Control

Lars Johannsmeier, Malkin Gerchow and Sami Haddadin

Institute of Automatic Control
Gottfried Wilhelm Leibniz Universität Hannover



<https://www.youtube.com/watch?v=ojpJIXliTYE>

Control Techniques for Serial Manipulator Robots

Classical Control, Machine Learning, and Reinforcement Learning



1. Classical Robotic Control

- Uses robot model and feedback
- PID control
- Computed torque / inverse dynamics
- Feedforward + feedback control
- Adaptive / robust control



Key idea: model-based control

★ Advantages: interpretable, stable, widely used



2. Machine Learning for Control

- Learns from data
- Neural network inverse model
- System identification
- Disturbance / friction estimation
- Imitation learning



Key idea: data-driven assistance or modeling

★ Advantages: handles nonlinearities and uncertainties



3. Reinforcement Learning Control

- Agent interacts with robot/environment
- State -> Action -> Reward
- Learns a control policy
- Trial-and-error improvement
- Useful for complex tasks



Key idea: learn by maximizing reward

★ Advantages: can learn complex behaviors

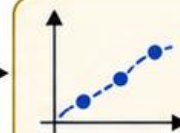


Desired Trajectory



Controller

Serial Manipulator Robot (6-DOF)



Measured Motion



Sensors / Encoders



Classical: relies on model



Machine Learning: relies on data



Reinforcement Learning: relies on interaction and reward



Goal: Generate control signals so the manipulator follows the desired trajectory accurately and robustly.

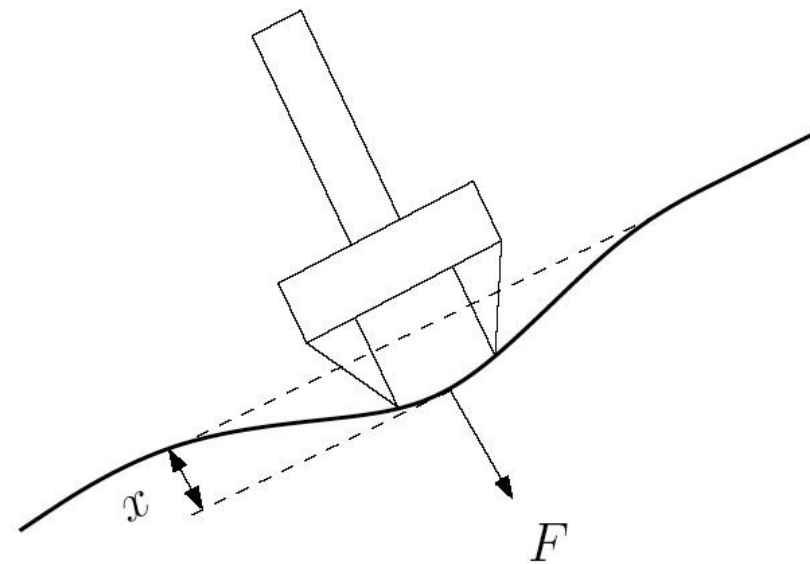
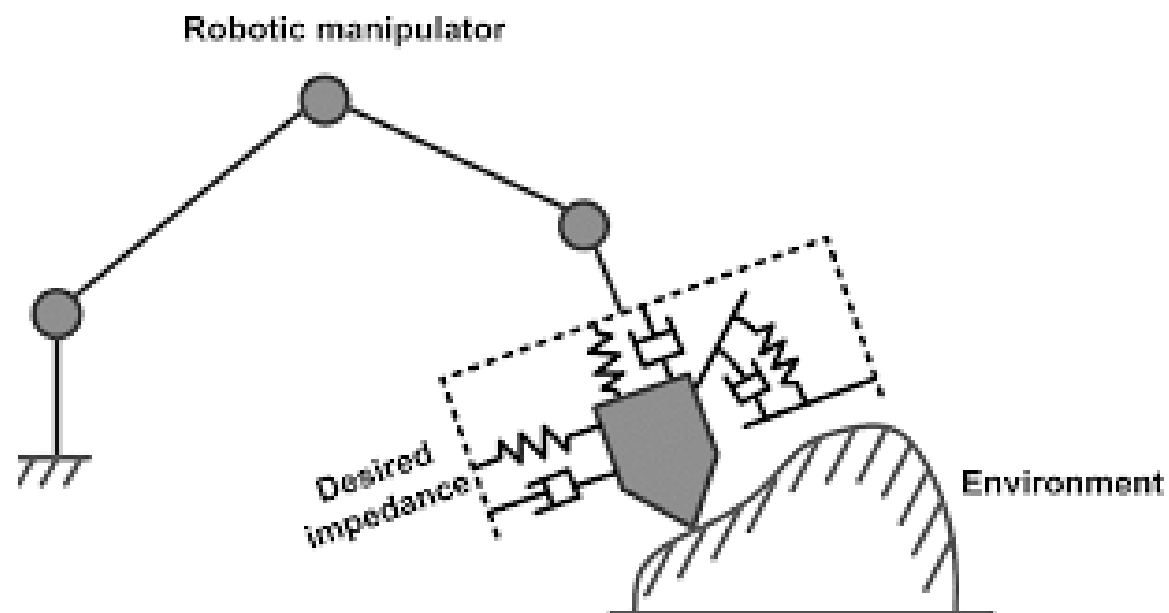
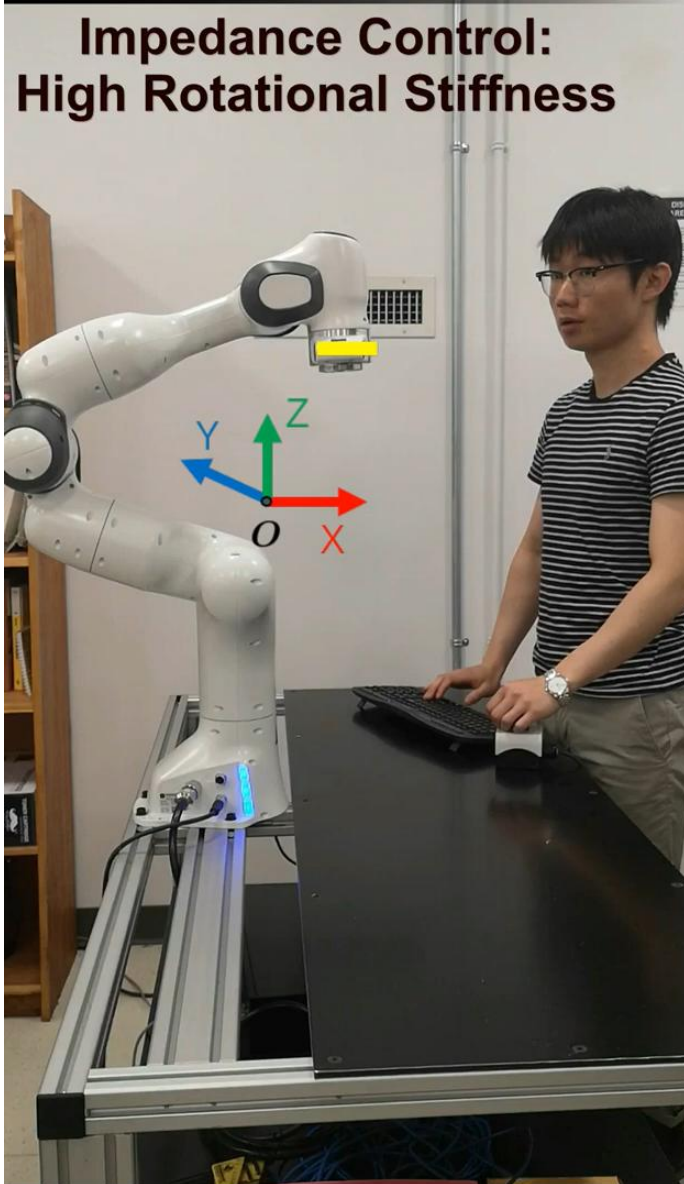


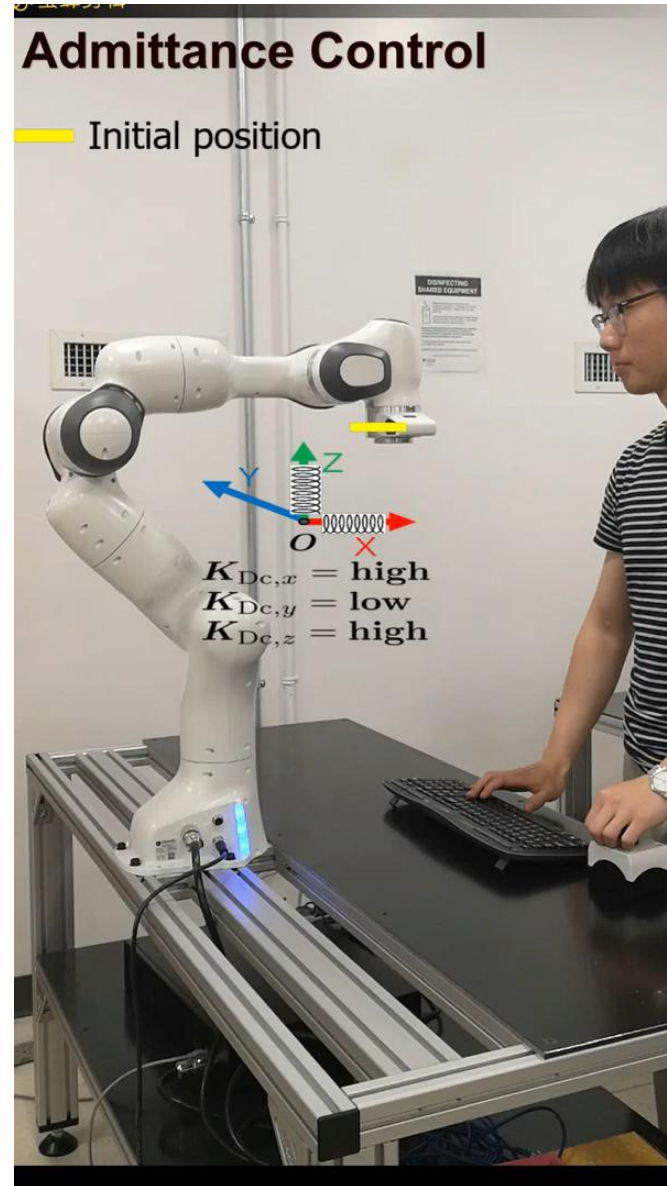
Figure 9.5: Compliant environment.



Impedance Control

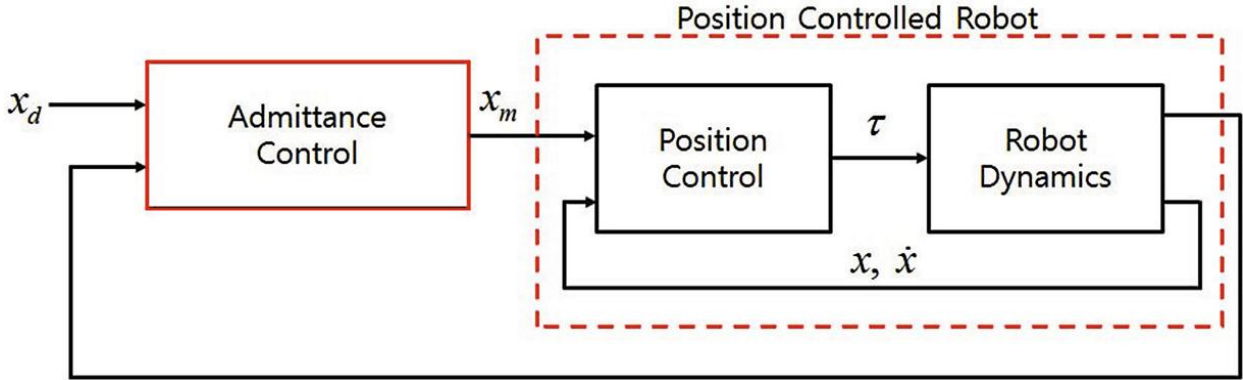
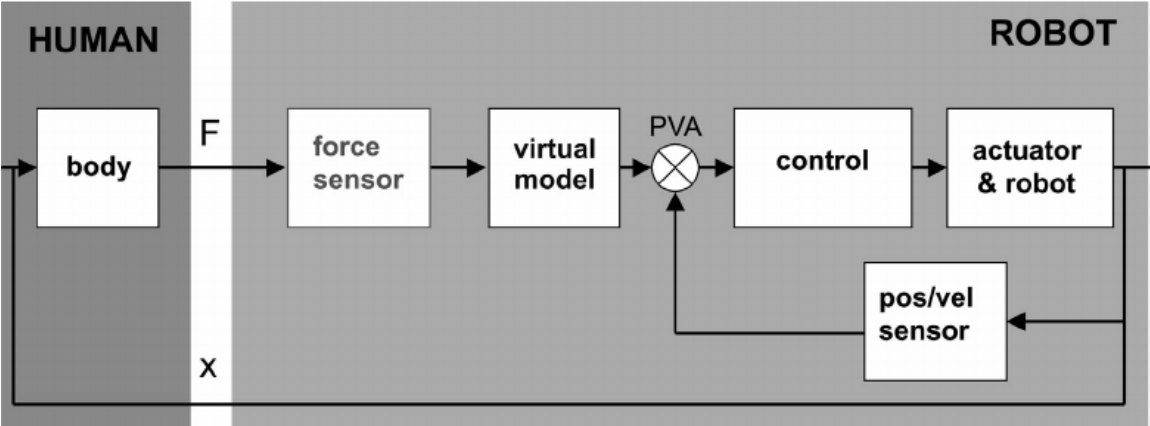
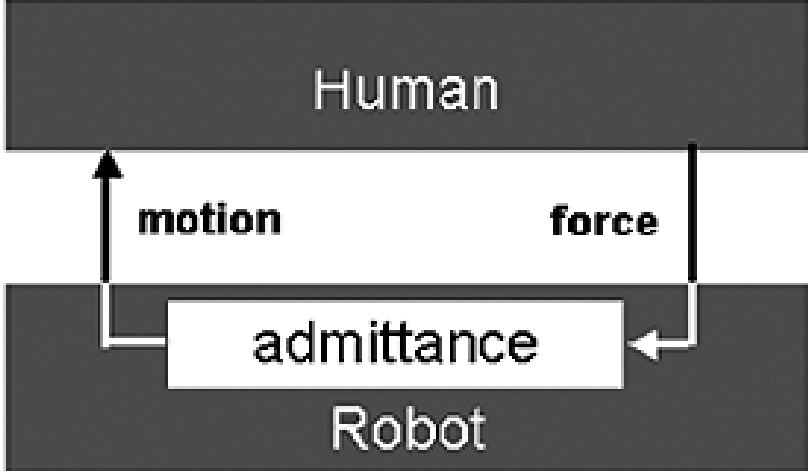
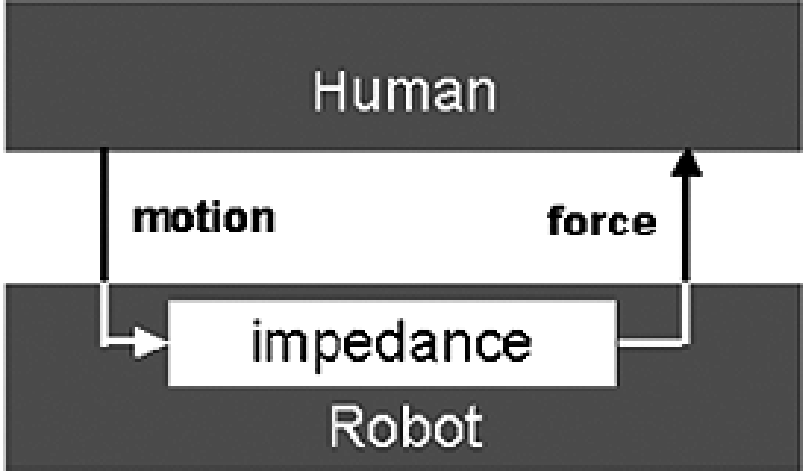


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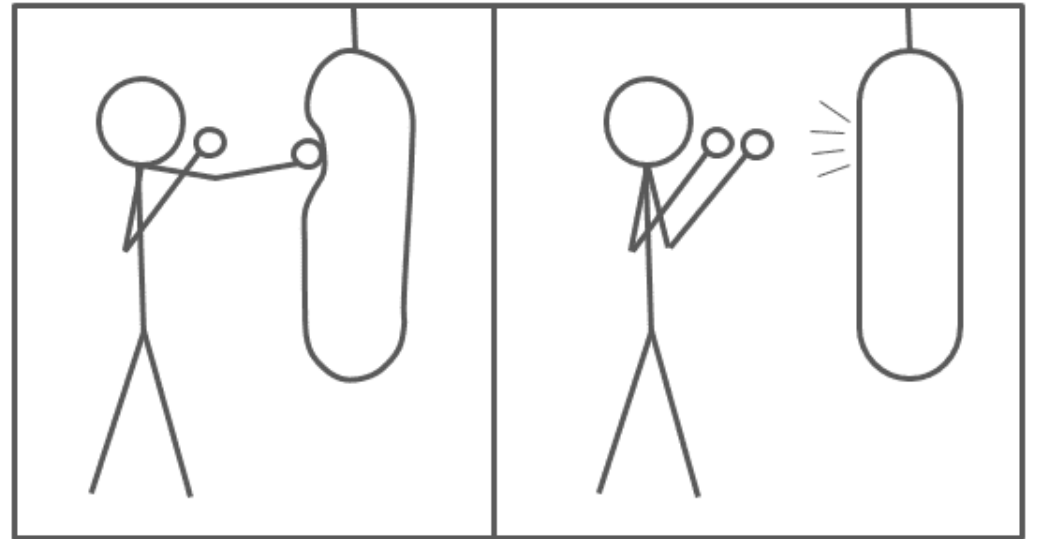
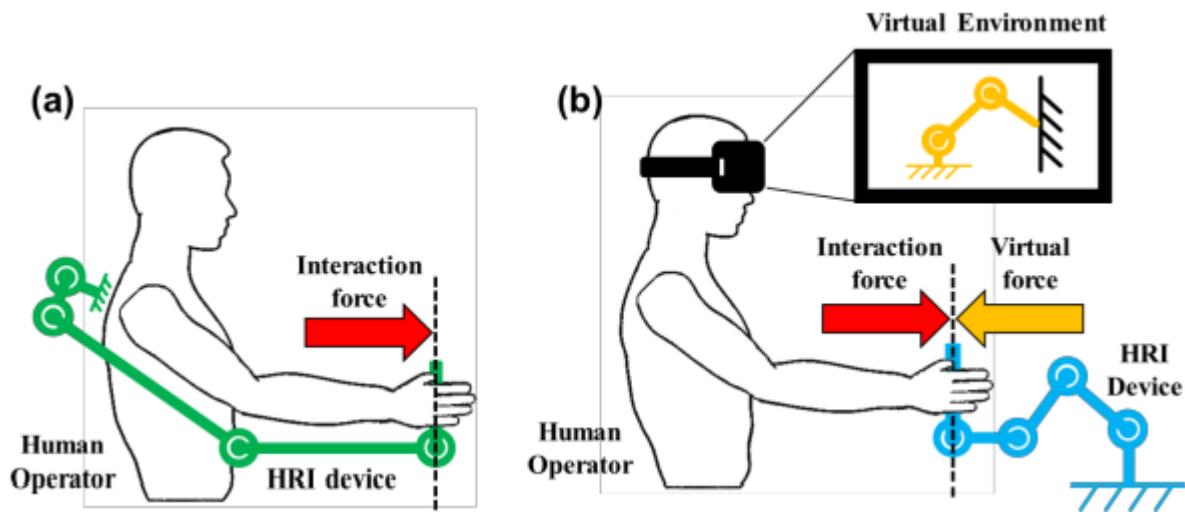
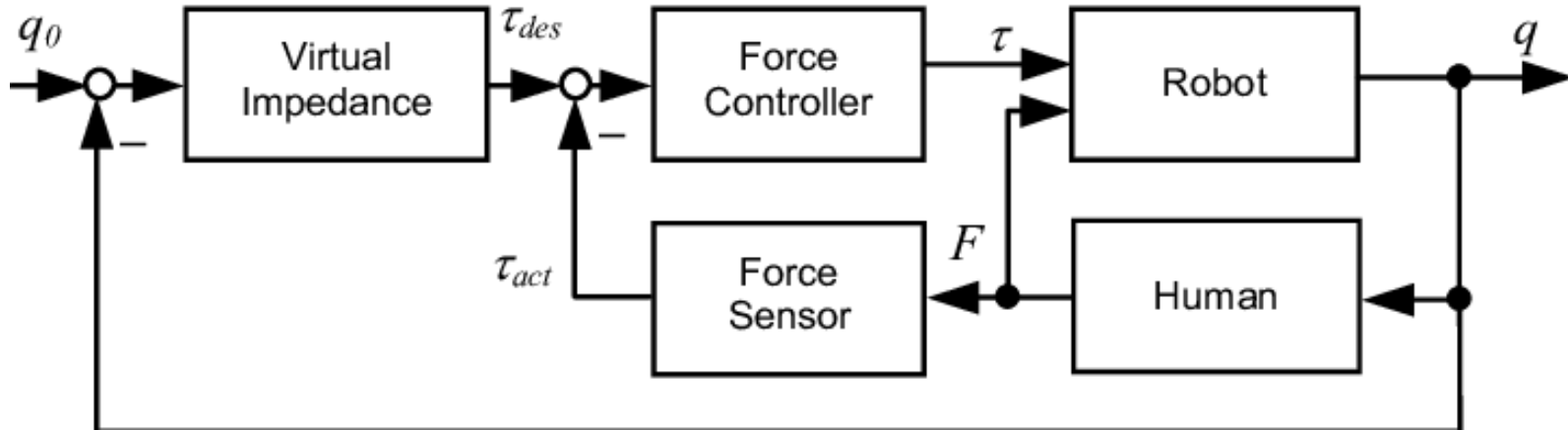


<https://www.youtube.com/shorts/cnFiTKgqB9M>

Impedance Control Vs Admittance Control



Impedance Control



Robot can be controlled to act as:

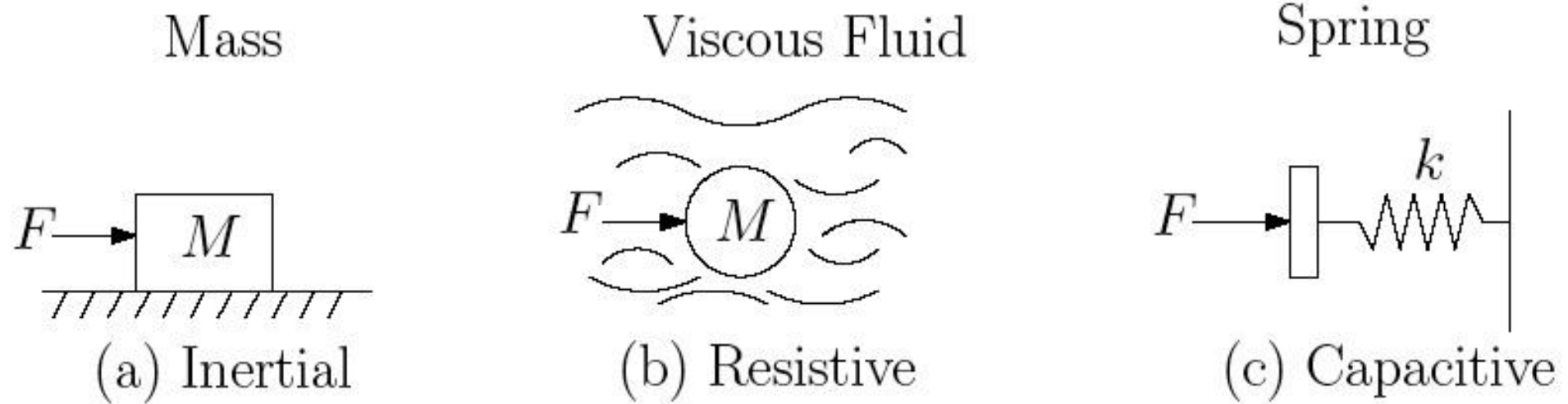
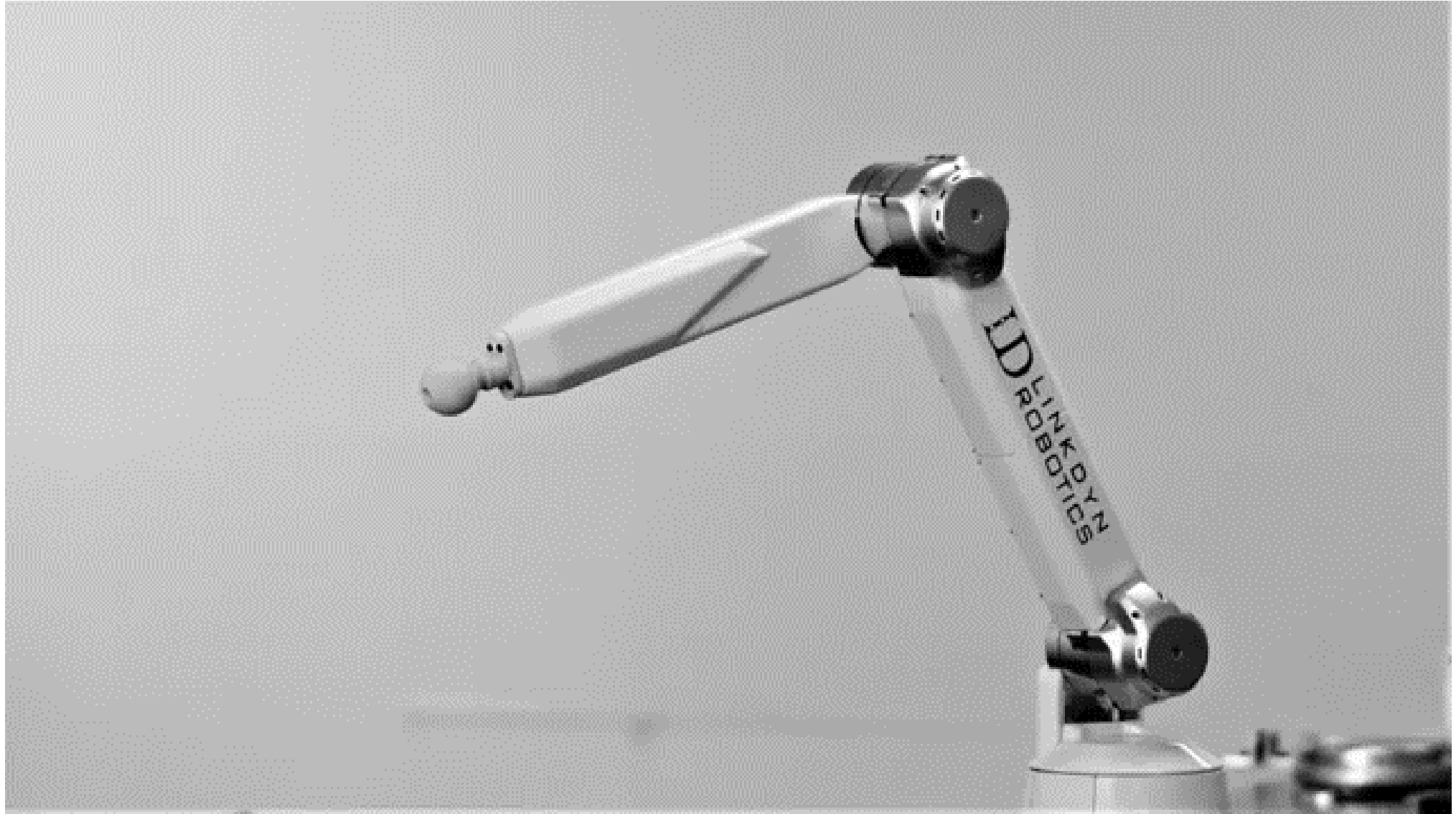


Figure 9.8: Examples of (a) inertial, (b) resistive, and (c) capacitive environments.

Physical Interaction robot



<https://www.youtube.com/watch?v=9H32TecFhY8>

Questions

Thank You